

# Highway Noise Analysis Report I-29 and 85th Street Interchange

Lincoln County, SD South Dakota DOT

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# Highway Noise Analysis Draft Report

## I-29 and 85th Street Interchange Project

Prepared for the South Dakota Department of Transportation (SDDOT).

## 1 Project Overview

The purpose of this analysis is to evaluate and document the effect of the proposed interchange improvements at I-29 and 85<sup>th</sup> Street and surrounding proposed local roadway improvements on traffic noise levels in the project area. The project area is located in Lincoln and Minnehaha Counties in South Dakota, and includes the Cities of Sioux Fall and Tea and Delapre Township.

## 1.1 Project Background and History

The City of Sioux Falls, in cooperation with SDDOT and the Sioux Falls Metropolitan Planning Organization (MPO), completed an Environmental Assessment (EA) in March of 2018 for the reconstruction of 85th Street between Sundowner Avenue and Louise Avenue and for the construction of an overpass at I-29. The Federal Highway Administration (FHWA) determined that the proposed improvements would have no significant impact on the human environment and issued a Finding of no Significant Impact (FONSI) on March 1, 2018. The Overpass EA did not include analysis or consideration for an interchange at I-29 and 85th Street. During the preparation of the Overpass EA, representatives of the 85th Street Joint Venture (JV) came forward with a request to evaluate an interchange at I-29 and 85th Street. In October 2018, the recommended interchange concept was accepted by FHWA. For additional project history and background, see Section 1 of the I-29 and 85th Street Interchange Environmental Assessment. Since the proposed interchange improvements qualify the project as a Type I project, a new traffic noise analysis was completed for incorporation into the new Environmental Assessment.

## 1.2 Project Description and Limits

The project includes the construction of a Diverging Diamond Interchange (DDI) along I-29 at 85<sup>th</sup> Street, including a connector ramp from southbound I-229 to the 85th Street exit ramp and a braided exit ramp from southbound I-29. The proposed action also includes the following improvements to the surrounding transportation system:

- Reconstruction of the I-229 NB exit ramp at S Louise Avenue as a two-lane exit ramp.
- Construction of an Auxiliary Lane on I-229 NB from the proposed 85th Street entrance ramp to the I-229 NB exit ramp at S Louise Avenue.
- Two-lane pavement of 270th Street from the proposed interchange at I-29 west to Ellis Road.
- Two-lane pavement of Sundowner Avenue from 69th Street to 270th Street.
- Two-lane pavement of 85<sup>th</sup> Street from S Tallgrass Avenue to S Louise Avenue.

The noise modeling limits include the following roadway limits: 469<sup>th</sup> Avenue to the west, S Louis Avenue to the east, the I-29/271<sup>st</sup> Street interchange to the south and various northern termini including I-229 NB auxiliary lane (proposed) to the I-229 NB exit ramp at S Louise Avenue, connector ramp from southbound I-229 to the 85th Street exit ramp and a braided exit ramp from southbound I-29.

It should be noted the roadway limits extend further than the project noise areas in order to capture the entire noise environment; the project noise areas are defined in **Section 5** of this report.

## 1.3 Project Assessment

This study was conducted in accordance with the Noise Analysis and Abatement Guidance for SDDOT (2011) and Federal Highway Administration (FHWA) Noise Regulation found at 23 CFR 772.

The analysis utilized FHWA's Traffic Noise Model 2.5 (TNM 2.5) software model. The analysis includes modeling of existing conditions (2015) and future (2045) build conditions.

## 2 Noise Overview

Noise is defined as any unwanted sound. Sound travels in a wave motion and produces a sound pressure level. This sound pressure level is commonly measured in decibels. For highway traffic noise, an adjustment, or weighting, of the high- and low-pitched sounds, is made to approximate the way that an average person hears sounds. The adjusted sound levels are stated in units of "A-weighted decibels" (dBA).

A-weighted decibels (dBA) represent the logarithmic increase (decrease) in sound energy relative to a reference energy level. A sound increase of 3 dBA is barely perceptible to the human ear, a 5 dBA increase is clearly noticeable, and a 10 dBA increase is heard as twice as loud. For example, if the sound energy is doubled (e.g., the amount of traffic doubles), there is a three dBA increase in noise, which is just barely noticeable to most people. On the other hand, if the traffic volumes increase by a factor of ten the sound energy level increases by 10 dBA, which is heard as a doubling of the loudness.

The following **Figure 1** provides a rough comparison of the noise levels of some common noise sources.

Figure 1 – Decibel Levels of Common Noise Sources

150	Jet take off (at close range on the ground)						
130	Machine gun, riveting machine						
120	Thunderclap						
117	jet plane (at passenger ramp)						
107	Loud power mower						
94	Pneumatic jackhammer						
90	Sports car, truck, shouted conversation						
50-60	Normal conversation						
50	Quiet street						
40	Quiet room						
0	Threshold of Audibility						

Source: "City Noise: Designers Can Restore Quiet, at a Price," by Harold W. Bredlin, *Product Engineering*, (November 1968) as cited in "The Audible Landscape: A Manual for Highway Noise and Land Use; Appendix B" (June 2017) Federal Highway Administration, https://www.fhwa.dot.gov

Along with traffic volumes, vehicle speeds, roadway grades, and topography, the distance of a receptor from a sound's source is also a significant factor that contributes to the level of traffic noise. Sound level decreases as the distance from the source increases. A general rule regarding sound level decrease due to increasing distance is: outside of approximately 50 feet, every time the distance between a line source, such as a roadway, and a receptor is doubled, the sound level decreases by either 3 dBA over hard surfaces or 4.5 dBA over soft surfaces.

## 2.1 Federal Regulations

The Federal Noise Abatement Criteria (23 CFR 772, Procedures for Abatement of Highway Traffic Noise and Construction Noise) established the noise criteria for various land uses. The criteria are in terms of the Leq descriptor. Leq is an equivalent steady-state sound level which contains the same acoustic energy as the time-varying sound level during the same time period.

Federal Noise Abatement Criteria (NAC) apply to all Type I projects requiring FHWA approval, regardless of funding source, or Type I projects requiring Federal-aid highway funds.

This project includes the construction of a new interchange at I-29 and 85<sup>th</sup> Street. The addition of a new interchange qualifies it as a Type I project. For the full definition of Type I projects see the definitions at link:

https://dot.sd.gov/media/documents/FinalNoiseAnalysisandAbatementGuidance071311.pdf

According to 23 CFR 772, a noise impact is defined as occurring when the predicted traffic noise levels:

- Approach or exceed the noise abatement criteria (see Table 1)
- Substantially exceed the existing noise levels

Table 1 – FHWA Noise Abatement Criteria

Activity Category	Activity Criteria <sup>1,2</sup> L <sub>eq</sub> (h) dBA	Evaluation Location	Activity Description
А	57	Exterior	Lands on which serenity and quiet are of extraordinary significance and serve an important public need and where the preservation of those qualities is essential if the area is to continue to serve its intended purpose
$B^3$	67	Exterior	Residential
C <sup>3</sup>	67	Exterior	Active sport areas, amphitheaters, auditoriums, campgrounds, cemeteries, day care centers, hospitals, libraries, medical facilities, parks, picnic areas, places of worship, playgrounds, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, recreation areas, Section 4(f) sites, schools, television studios, trails, and trail crossings
D	52	Interior	Auditoriums, day care centers, hospitals, libraries, medical facilities, places of worship, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, schools, and television studios
E <sup>3</sup>	72	Exterior	Hotels, motels, offices, restaurants/bars, and other developed lands, properties or activities not included in A-D or F
F	l		Agriculture, airports, bus yards, emergency services, industrial, logging, maintenance facilities, manufacturing, mining, rail yards, retail facilities, shipyards, utilities (water resources, water treatment, electrical), and warehousing
G			Undeveloped lands that are not permitted.

#### Notes:

- (1) Leq(h) shall be used for impact assessment
- (2) Leq(h) Activity Criteria values are for impact determination only, and are not design standards for noise abatement
- (3) Includes undeveloped lands permitted for this activity category

## 2.2 | State Regulations

South Dakota DOT has defined "approach or exceed" as when the predicted Leq is within one dBA, or less, or exceeds the Leq given for the activity category in the NAC (Table 1), and "substantially exceed" as an increase of 15 dBA or more over existing noise levels.

In South Dakota, traffic noise impacts are evaluated by measuring and/or modeling the traffic noise levels that exceed the equivalent steady-state sound level of the time during the worst hour traffic volumes for the design year. This number is identified as the Leq levels; the Leq value is compared to FHWA noise abatement criteria.

## 3 Methodology

## 3.1 Affected Environment

The purpose of this noise analysis is to determine the impacts the proposed project has on traffic noise levels in the immediate vicinity of the project at noise sensitive receptors (residences,

businesses, etc). It is important to note that this analysis only includes traffic generated noise. There are other noise sources in the project area that have some effect on the ambient noise levels.

The project will construct a diverging diamond interchange at I-29 and 85<sup>th</sup> Street, as well as various other roadway improvements associated with the project.

## 3.2 | Field Monitoring

Noise level monitoring is required for noise studies to document existing noise levels and assist in validating the noise prediction model. Monitored noise levels can also be used as a baseline of the possible ambient noise levels that can occur with a new roadway alignment.

The existing noise levels in the I-29/85<sup>th</sup> Street project area were monitored at four sites on July 2<sup>nd</sup>, 2019. The monitoring location sites are illustrated in **Figure 2**, Existing Conditions. The four sites were selected to have field measurements done, to capture existing noise along the study limits; most of the project area where proposed improvements occur are undeveloped or very few sensitive receptors nearby. Site M1 was selected based on the close proximity to the large number of homes on the northwest side of the project area. Site M2 was selected based on the close proximity to the existing I-29 traffic and to represent the few homes still left along the west side of I-29. Site M3 was selected to represent sensitive receptors on the east side of the I-29, along 85th Street. Site M4 was selected to represent sensitive receptors located at/near the Avera hospital location and because of its close proximity to existing I-229 traffic.

Short-term noise measurements of 30 minutes were conducted at each of these locations and were used to validate the model. Concurrent traffic data was collected for the duration of each monitoring session, which was then used to develop hourly volumes for each site for the validation model. The noise level monitoring results are shown on the monitoring summary sheets in **Appendix D**, and ranged from 53.1 dBA (L<sub>eq</sub>) to 64.6 dBA (L<sub>eq</sub>). The monitoring time periods had good weather (no precipitation with winds less than 12 mph), and dry pavement; the sound level meter utilized was a Larson Davis model 831 that was laboratory calibrated in March of 2019.

Field data sheets were generated for each site, including collected traffic data, weather, wind speed, time and location of measurement, as well as any other observed noise sources that occurred during the measurement. Field data sheets and photographs of each measurement location and can be found in **Appendix D**.



Figure 2 – Existing Conditions – Monitor Locations and Project Area

## 3.3 Noise Model Validation

The noise modeling for both the existing noise levels and future build noise levels was done using the noise prediction program TNM 2.5, which was developed for FHWA. The model uses the roadway alignment (horizontal and vertical), traffic volumes, traffic speeds, vehicle classification, and the distances from the roadway center-of-lanes to the receptors as well as

relative elevation differences. In general, higher traffic volumes, vehicle speeds, and numbers of heavy trucks increases the loudness of highway traffic noise.

To verify the accuracy of the noise model, the modeled noise level results must be within +/- 3 dBA of the monitored noise levels (*Highway Traffic Noise: Analysis and Abatement Guidance*, Federal Highway Administration, Washington, DC, December 2011, pp. 31–32). The monitoring results are provided in **Table 2**, which shows the results of the validation modeling to be within the 3 dBA limits for the Leq for 3 of the 4 sites. The modeled results for Site M1, near 69<sup>th</sup> Street and Sundowner Avenue, was 6.1 dBA lower than what was measured at the site. This difference is attributed to the ambient noise surrounding the site at the time of monitoring being louder than the noise generated by the nearby traffic, especially since there was very little traffic occurring near this site during the monitoring session. Also, during the field monitoring, it was observed that the air conditioners were audible from the nearby homes at the monitoring location and there were 3 instances of water trucks with back-up beepers going during the monitoring, as well as an audible airplane overhead. All of these events contributed to the difference in the validation results at this location. It is important to note that the TNM 2.5 program only accounts for noise generated from vehicles and not background noise. Since the other three sites were within 3 dBA difference between the measured and modeled results, the model is considered validated.

Site	Location/Description	Measurement	Measured Levels, dBA	Modeled Levels, dBA	Difference dBA
ID		Date/Time	Leq	Leq	Leq
M1	NE Quadrant of 69 <sup>th</sup> Street and Sundowner Avenue	July 2, 2019 10:10 am to 10:40 am	53.9	47.8	-6.1
M2	At 270 <sup>th</sup> Street and I-29 (West of I-29 SB)	July 2, 2019 11:02 am to 11:32 am	64.6	67.1	+2.5
М3	At NW Quadrant of 85 <sup>th</sup> Street and Tallgrass Avenue	July 2, 2019 12:04 am to 12:34 am	53.1	51.3	-1.8
M4	At Avera Hospital Grounds (South of I-229 EB)	July 2, 2019 1:13 pm to 1:43 pm	64.6	62.3	-2.3

Table 2 – Noise Monitoring Locations & Results

# 4 Noise Analysis .1 Noise Modeling

Traffic noise impacts were assessed by modeling noise levels at noise sensitive receptor locations likely to be affected by the construction of the proposed project. SDDOT Noise Analysis and Abatement Guidance defines the noise study area for the build alternative to be from the beginning project construction point to the ending project construction point. The minimum distance to look for receptors is 300 feet from the edge of pavement. If an impact is identified at 300 feet, the next closest receptor would need to be analyzed until a distance where impacts are no longer identified is reached. If no receptors are located within the 300 foot zone, then the closest receptor(s) should be analyzed.

The project receptors were divided up into 15 separate noise areas based on proximity of adjacent receptors and roadway access locations, as shown in **Appendix A Figure 1**; **Noise Analysis Overview Map.** Using worst hour traffic volumes for the design year and future posted

speed limits, traffic noise levels were modeled at a total of 169 representative receptor locations throughout the project area. The majority of the receptors represent residential receptors located throughout the project area, with the exception of two medical facilities, three commercial properties, and an elementary school. The locations of the existing and future build modeled receptor sites are illustrated in **Appendix C Figures 1 through 6**; Noise Analysis Future Build and Barrier Results.

The attached **Table 3** includes the predicted results, receptor site ID and land use for each receptor.

The following assumptions were used in modeling the noise levels for this project:

- Traffic data input into the noise model included Existing (year 2015) and Build (year 2045) forecast traffic volumes from the Intersection Justification Report (IJR). Year 2045 was identified as the design year for the proposed project.
- Existing 24-hour vehicle data was used to determine that the peak hourly traffic occurs between 4:45 p.m. and 5:45 p.m.
- Vehicular fleet composition was determined based on truck percentages generated for the IJR and from traffic counts collected during field monitoring.

#### 4.2 Noise Model Results

Results of the noise modeling analysis are tabulated in the attached **Table 3**, **Noise Analysis Summary Table**. The following describes the results of the traffic noise analysis for existing (2015) and future (2045) Build condition.

Existing (2015) modeled noise levels at the modeled receptor locations range from 37.0 dBA (L<sub>eq</sub>) to 68.2 dBA (L<sub>eq</sub>). Modeled noise receptors exceeded FHWA Noise Criteria (L<sub>eq</sub>) at 1 of 167 modeled receptor locations under existing (2015) conditions.

Future (2045) Build modeled noise levels at the modeled receptor locations range from 42.0 dBA ( $L_{eq}$ ) to 70.7 dBA  $L_{eq}$ ). Modeled noise receptors exceeded FHWA criteria ( $L_{eq}$ ) at 65 of 167 modeled receptor locations under Build (2045) conditions, with 29 of these being from a "substantial increase" in traffic noise due to the proposed project.

Modeled noise level changes range from 0.5 dBA to 20.7 dBA for existing receptor locations when comparing the Build (2045) to the existing (2015) conditions.

Generally, traffic noise levels are increased with the proposed build project due to many factors. A few of the major changes that influence the increases are as follows:

- Traffic demands will increase between the existing (2015) conditions and future (2045) conditions.
- The proposed 85<sup>th</sup> Street interchange will create new access to I-29, which will direct new traffic along 85<sup>th</sup> Street.
- Additional residential development will continue along 85<sup>th</sup> Street, east of the proposed interchange

## 5 | Noise Abatement Analysis

Because Federal Noise Abatement Criteria (NAC) are both approached and exceeded at modeled receptor locations throughout the project area, noise abatement must be considered.

Noise mitigation measures have been considered, as listed in 23 CFR 772.13(c) and are addressed below:

- Traffic management measures: The primary purpose of the facility is to move people and goods. Restrictions of certain vehicles or speeds would be inconsistent with the purpose of the project.
- Alteration of horizontal and vertical alignments: The proposed interchange location was selected based on the proposed demands for existing and proposed land use. The majority of current land use where the proposed interchange will be constructed is open space. Adjacent land use is primarily residential, which will provide people with alternate access to the I-29/I-229 interchange. Redesigning the horizontal and vertical alignments to minimize noise impacts would be impractical for this project.
- Acquisition of real property or interests therein (predominantly unimproved property) to serve as a buffer zone to preempt development that would be adversely impacted by traffic noise: Exclusive land use designations or acquisition of property to serve as a buffer zone between the roadway and adjacent lands would not be feasible because land has already been developed along the project corridor.
- Noise insulation of public use or nonprofit institutional structures: Under FHWA
  guidelines, only public buildings such as schools and hospitals should be considered for
  acoustical insulation. Within the project area, there is not a noise exceedance near the
  buildings' location for these types of land uses.
- Construction of Noise Barriers: including acquisition of property rights, either within or outside the highway right of way.

Noise barriers have been chosen as the most cost-effective noise mitigation measure available for this project.

The use of quieter pavements is not an acceptable noise abatement measure for Federal-aid projects. Planting of vegetation or landscaping is not an acceptable Federal-aid noise abatement measure because only dense stands of evergreen vegetation at least 100 feet deep will reduce noise levels by a noticeable amount.

#### 5.1 Noise Barrier Evaluation

When noise impacts are identified, a noise barrier evaluation analysis must be performed. Noise barrier construction decisions are determined based on the evaluation of the feasibility and reasonableness of the noise barriers.

Feasibility of the noise barrier is determined by engineering feasibility (i.e., whether a noise barrier could feasibly be constructed on the site) and by acoustic feasibility (a minimum of 60% of front row receptors directly behind the noise wall achieve a 5 dBA noise reduction). The feasibility of noise barrier construction is sometimes dependent on design details that are not known until the final design of the project. The following analysis assumes that noise barriers could be feasibly constructed throughout the project area, up to 20 feet high along the corridor.

Reasonableness is based on three factors determined by the number of benefited receptors from the noise abatement that must be met. A benefited receptor is any receptor behind the noise

barrier that receives a minimum noise level reduction of 5 dBA or more. The three reasonableness factors are as follows:

- A cost effectiveness (CE) threshold of \$21,000 per individual benefited receptor has been
  established, based on an estimated construction cost of \$44 per square foot for noise
  barriers. The cost calculations for the noise abatement measure should include all items
  directly related to the construction of the noise abatement measure, including additional
  costs of some items such as right-of-way, drainage modifications, utility relocation, traffic
  control, retaining walls, landscaping for graffiti abatement and standard aesthetic
  treatments.
- At least 40% of benefited receptors must achieve a 7 dBA noise reduction in order for noise abatement to be reasonable.
- The viewpoints of the property owners and residents of all benefited receptors shall be solicited and considered in reaching a decision on the abatement measure to be provided. See Section 9 of the SDDOT Noise Analysis and Abatement Guidance (effective date: July 13, 2011) for a detailed explanation of the voting system.

All barriers evaluated must meet SDDOT's 7 dBA noise reduction design goal for at least 40% of the benefited receptors for each noise abatement measure evaluated. If a barrier is unable to achieve the design goal, further evaluation will not be completed.

#### 5.1.1 Project Summary

Federal Noise Abatement Criteria (NAC) are currently predicted to be both approached and exceeded throughout portions of the study area. Noise barriers were evaluated at 10 barrier locations within the project's 15 noise areas. **Appendix C Build Condition Figures 1-6** illustrates the analysis summary of noise barriers that were considered.

Noise barrier cost-effectiveness results are tabulated in **Appendix B Noise Barrier Tables**.

## 5.1.2 Vehicle Sight Lines

Along 85<sup>th</sup> Street, there are side street stop control access locations and driveways. Intersection sight lines were evaluated at each access point to determine where any proposed barrier must not encroach, to ensure propose and safe sight lines for all users. Barriers would need to follow along the sight line, requiring additional right-of-way and/or easements. Based on the American Association of State Highway and Transportation Officials (AASHTO) Guide, at 40 mph, sight distance requirements for left-turning single-unit vehicles from the minor, stop-controlled road is 685 feet, for Beal Avenue and Tuscan Club Circle.

There are multiple residences along 270<sup>th</sup> Street and 85<sup>th</sup> Street where the only direct access to those residences is those roadways. Since access will need to be maintained for these homes, there are some impacted residences where noise barriers were not considered feasible.

## 5.2 Noise Barrier Results

The previous Overpass EA analyzed eight noise areas for noise abatement based on the receptors surrounding the overpass construction limits, located along 270<sup>th</sup> Street and 85<sup>th</sup> Street. Abatement for seven of the noise areas were found to be either not feasible or not reasonable.

The project receptors were divided up into 15 separate noise areas based on proximity of adjacent receptors and highway access locations (see **Figure 1** in **Appendix A**).

#### 5.2.1 Noise Area 1 – Sundowner Avenue (West)

Land uses west of Sundowner Avenue consist of 1 residential receptor. The proposed project in this noise area will pave Sundowner Avenue along its existing profile.

Noise levels were modeled at 1 receptor location in Noise Area 1. Modeled noise levels approached or exceeded the Federal NAC at 0 of 1 receptor locations with future (2045) Build conditions. With no impacted receptor in Noise Area 1, no mitigation was evaluated for this noise area.

#### 5.2.2 Noise Area 2 – Sundowner Avenue (East)

Land uses east of Sundowner Avenue consist of 2 residential receptors. The proposed project in this noise area will pave Sundowner Avenue along its existing profile.

Noise levels were modeled at 2 receptor locations in Noise Area 2. Modeled noise levels had a significant increase impact at Receptor 2-1 with future (2045) Build conditions. Noise abatement at this receptor was not feasible due to the need of direct access to the property off Sundowner Avenue. No mitigation was evaluated for this noise area.

#### 5.2.3 Noise Area 3 – South of I-229 Northbound

Land uses south of I-229 Northbound consist of non-residential hospital facilities on the south side of I-229. The proposed project in this noise area constructs an auxiliary lane from 85<sup>th</sup> Street entrance ramp to I-229 northbound exit ramp at Louise Avenue, along the existing edge of pavement.

Noise levels were modeled at 4 receptor locations in Noise Area 3. Receptors 3-3 and 3-4 represents exterior land use at the Encompass Health Rehabilitation Hospital of Sioux Falls, which is currently under construction. Modeled noise levels approached or exceeded the Federal NAC at 0 of 4 receptor locations with future (2045) Build conditions.

#### 5.2.4 Noise Area 4 – South of I-229 NB Exit Ramp at Louise Avenue

Land uses south of I-229 Northbound exist ramp at Louise Avenue consist of commercial buildings on the south side of the Louise Avenue ramp. The proposed project in this noise area constructs an auxiliary lane from 85<sup>th</sup> Street entrance ramp to I-229 northbound exit ramp at Louise Avenue, along the existing edge of pavement.

Noise levels were modeled at 3 receptor locations in Noise Area 4. Modeled noise levels approached or exceeded the Federal NAC at 0 of 3 receptor locations with future (2045) Build conditions.

## 5.2.5 Noise Area 5 – 270th Street (between Ellis Road and Sundowner Avenue)

Land uses along 270<sup>th</sup> Street, between Ellis Road and Sundowner Avenue consists of 2 residential receptors. The proposed project in this noise area will pave Sundowner Avenue along its existing profile.

Noise levels were modeled at 2 receptor locations in Noise Area 5. Modeled noise levels had a significant increase impact at Receptor 5-1 with future (2045) Build conditions. Noise abatement at this receptor was not feasible due to the need of direct access to the property off 270<sup>th</sup> Street. No mitigation was evaluated for this noise area.

#### 5.2.6 Noise Area 6 – Sundowner Avenue (North of 270th Street)

Land uses along Sundowner Avenue, north of 270<sup>th</sup> Street consists of 3 residential receptors. The proposed project in this noise area will pave Sundowner Avenue along its existing profile.

Noise levels were modeled at 3 receptor locations in Noise Area 6. Modeled noise levels approached or exceeded the Federal NAC at 0 of 3 receptor locations with future (2045) Build conditions.

#### 5.2.7 Noise Area 7 – 270<sup>th</sup> Street (Between Sundowner Avenue and Interchange)

Land uses along 270<sup>th</sup> Street, between Sundowner Avenue and the proposed I-29 interchange consists of 6 residential receptors. The proposed project in this noise area will widen 270<sup>th</sup> Street, providing two through-lanes and right and left turn lanes on all approaches. The intersection of 270<sup>th</sup> Street and Sundowner Avenue will also be signalized.

Noise levels were modeled at 5 receptor locations in Noise Area 7. Modeled noise levels had a significant increase impact at Receptors 7-1 and 7-2 with future (2045) Build conditions. Noise abatement at these receptors was not feasible due to the need of direct access to the property off 270<sup>th</sup> Street. No mitigation was evaluated for this noise area. Receptors 7-4 and 7-5 will be demolished during the proposed design.

## 5.2.8 Noise Area 8 – 85th Street North (Interchange to Tallgrass Avenue)

Land uses along the north side of 85<sup>th</sup> Street, from the proposed I-29 interchange to Tallgrass Avenue consists of 4 residential receptors. The proposed project in this noise area will raise the profile at the 85<sup>th</sup> Street/Tallgrass Avenue intersection, widen 85<sup>th</sup> Street and Tallgrass to accommodate two through-lanes, right and left turn lanes on all approaches. The intersection will also be signalized.

Noise levels were modeled at 4 receptor locations in Noise Area 8. Modeled noise levels approached or exceeded the Federal NAC at 3 of 4 receptor locations with future (2045) Build conditions. Noise abatement at these receptors was not feasible due to the need of direct access to the property off 85<sup>th</sup> Street. No mitigation was evaluated for this noise area. Receptor 8-1 will be demolished during the proposed design.

## 5.2.9 Noise Area 9 – 85<sup>th</sup> Street North (Tallgrass Avenue to Beal Avenue)

Land uses along the north side of 85<sup>th</sup> Street, from Tallgrass Avenue to Beal Avenue consists of residential receptors, including multiple single family homes and townhouse complexes. The proposed project in this noise area will lower the profile along 85<sup>th</sup> Street approximately 2-3 feet, widen 85<sup>th</sup> Street and Tallgrass to accommodate two through-lanes, right and left turn lanes and signalize the intersections of Tallgrass Avenue, Townsley Avenue, and Beal Avenue.

Noise levels were modeled at 21 receptor locations in Noise Area 9. Modeled noise levels approached or exceeded the Federal NAC at 13 of 21 receptor locations with future (2045) Build conditions.

For receptors 9-2, 9-6, 9-7 and 9-8, modeled noise levels had a significant increase impact with future (2045) Build conditions. Noise abatement at these receptors was not feasible due to the need of direct access to the property off 85<sup>th</sup> Street. No mitigation was evaluated for this noise area.

For receptors 9-4 and 9-5, modeled noise levels had a significant increase impact with future (2045) Build conditions. Since receptors 9-4 and 9-5 both have direct access off Cactus Place, a noise barrier was modeled along both parcels on 85<sup>th</sup> Street.

For receptors 9-9A, 9-9B, 9-10 and 9-11, modeled noise levels exceeded the Federal NAC with the future build, while receptors 9-13, 9-14, and 9-17 had a significant increase impacts with future (2045) Build conditions. A noise barrier was modeled behind the proposed sidewalk location along 85<sup>th</sup> Street to mitigate traffic noise to these multi-family dwellings.

#### 5.2.9.1 Barrier 9-1

An approximately 170 foot long, 15 foot high noise barrier was modeled on the north side of 85<sup>th</sup> Street, east of Tallgrass Avenue, to mitigate impacts to the residential receptor "9-4". The barrier provides a reduction of 2.3 dBA for receptor 9-4 and 0.7 dBA reduction for receptor 9-3. Iterating the barrier height higher did not provide any additional noise reduction. The noise barrier does not meet SDDOT's 7 dBA noise reduction design goal and is therefore not proposed.

#### 5.2.9.2 Barrier 9-2

An approximately 180 foot long, 16 foot high noise barrier was modeled on the north side of 85<sup>th</sup> Street, east of Tallgrass Avenue, to mitigate impacts to the residential receptor "9-5". The barrier provides a reduction of 2.2 dBA. Iterating the barrier height higher did not provide any additional noise reduction. The noise barrier does not meet SDDOT's 7 dBA noise reduction design goal and is therefore not proposed.

#### 5.2.9.3 Barrier 9-3

An approximately 235 foot long, 6 foot high noise barrier was modeled on the north side of 85<sup>th</sup> Street, east of Tallgrass Avenue, to mitigate impacts to the residential receptors 9-9A, 9-9B, 9-10, 9-11, 9-13, 9-14 and 9-17. The barrier provides a reduction that varies from 0.2 to 9.2 dBA. 5 out of 5 (100%) of the benefited receptors achieve a noise reduction of 7.0 dBA or more. Due to limited existing right-of-way, the proposed barrier layout will require the purchase of easements. The cost of the proposed barrier with the proposed easements (10 feet behind the barrier) is \$18,355 per benefited receptor. Since the barrier design meets both reasonableness and feasibility requirements, the noise barrier will be presented to the benefited residents and owners for voting as outlined in the SDDOT Noise Analysis and Abatement Guidance (effective date: July 13, 2011).

### 5.2.10 Noise Area 10 – 85th Street North (Beal Avenue to Hughes Avenue)

Land use along the north side of 85<sup>th</sup> Street, from Beal Avenue to Hughes Avenue consists of residential receptors, consisting of multiple single family homes and townhouse complexes. The proposed project in this noise area will lower the profile along 85<sup>th</sup> Street approximately 2-3 feet, widen 85<sup>th</sup> Street and Tallgrass to accommodate two through-lanes, right and left turn lanes and signalize the intersections of Beal Avenue and Hughes Avenue.

Noise levels were modeled at 31 receptor locations in Noise Area 10. Modeled noise levels approached or exceeded the Federal NAC at 17 of 31 receptor locations with future (2045) Build conditions.

#### 5.2.10.1 Barrier 10-1

An approximately 1,387 foot long, 6 foot high noise barrier was modeled on the north side of 85<sup>th</sup> Street, east of Beal Avenue, to mitigate impacts to the residential receptors 10-1 through 10-14 and 10-28 through 10-30. The barrier provides a reduction that varies from 2.6 to 8.3 dBA. 7 out of 13 (54%) of the benefited receptors achieve a noise reduction of 7.0 dBA or more. However, the cost per benefited receptor is \$28,167, which exceeds the allowable CE threshold of \$21,000 benefited receptor.

A second alternative noise barrier design was modeled of the same 1,387 foot length, but that had a more cost-effective average height of 5.4 feet, to mitigate impacts to the residential receptors 10-1 through 10-14 and 10-28 through 10-30. The barrier provides a reduction that varies from 2.4 to 7.5 dBA. Only 5 out of 13 (38%) of the benefited receptors achieve a noise reduction of 7.0 dBA or more, which does not meet the 7.0 dBA or more noise reduction goal for 40% of benefited receptors. Also, the cost per benefited receptor is \$25,397, which exceeds the allowable CE threshold of \$21,000 benefited receptor and therefore, is not proposed.

#### 5.2.11 Noise Area 11 – 85<sup>th</sup> Street North (Hughes Avenue to S Louise Avenue)

Land uses along the north side of 85<sup>th</sup> Street, from Hughes Avenue to S Louise Avenue consists of residential receptors, consisting of multiple single family homes. The proposed project in this noise area will lower the profile approximately 1 foot in some areas along 85<sup>th</sup> Street. 85<sup>th</sup> Street will be widened to accommodate two through-lanes, right and left turn lanes at Hughes Avenue and signalize the intersection of Hughes Avenue.

Noise levels were modeled at 22 receptor locations in Noise Area 11. Modeled noise levels approached or exceeded the Federal NAC at 4 of 22 receptor locations with future (2045) Build conditions.

#### 5.2.11.1 Barrier 11-1

An approximately 745 foot long, 6.4 foot high noise barrier was modeled on the north side of 85<sup>th</sup> Street, east of Hughes Avenue, to mitigate impacts to the residential receptors 11-1 through 11-4. The barrier provides a reduction that varies from 0.5 to 7.7 dBA. 3 out of 6 (50%) of the benefited receptors achieve a noise reduction of 7.0 dBA or more. However, the cost per benefited receptor is \$34,801, which exceeds the allowable CE threshold of \$21,000 benefited receptor.

A second alternative noise barrier design was modeled of the same 745 foot length, but that had a more cost-effective average height of 5.7 feet, to mitigate impacts to the residential receptors 11-1 through 11-4. The barrier provides a reduction that varies from 0.4 to 7.0 dBA. Only 1 out of 6 (17%) of the benefited receptors achieve a noise reduction of 7.0 dBA or more, which does not meet the 7.0 dBA or more noise reduction goal for 40% of benefited receptors. Also, the cost per benefited receptor is \$30,977, which exceeds the allowable CE threshold of \$21,000 benefited receptor and therefore, is not proposed.

## 5.2.12 Noise Area 12 – 85<sup>th</sup> Street South (Townsley Avenue to Brett Avenue)

Land uses along the south side of 85<sup>th</sup> Street, from Townsley Avenue to Brett Avenue consist of residential receptors, including multiple townhouse complexes. The proposed project in this noise area will lower the profile along 85<sup>th</sup> Street approximately 2-3 feet, widen 85<sup>th</sup> Street and Townsley Avenue to accommodate two through-lanes, right and left turn lanes and signalize the intersections of Townsley Avenue and Brett Avenue.

Noise levels were modeled at 29 receptor locations in Noise Area 12. Modeled noise levels approached or exceeded the Federal NAC at 14 of 29 receptor locations with future (2045) Build conditions.

#### 5.2.12.1 Barrier 12-1

An approximately 650 foot long, 6 foot high noise barrier was modeled on the south side of 85<sup>th</sup> Street, west of Brett Avenue, to mitigate impacts to the residential receptors 12-1 through 12-11 and 12-13 through 12-15. The barrier provides a reduction that varies from 0.1 to 9.2 dBA. 14 out of 15 (93%) of the benefited receptors achieve a noise reduction of 7.0 dBA or more. The cost per benefited receptor for the barrier alone is \$11,440. However, the proposed barrier would be located along the Lewis & Clark waterline and within the Lewis & Clark permanent utility easement, making construction of this barrier not feasible. Approximately 650 feet of this utility would be impacted by the construction of the barrier. Additional costs incurred from relocating the waterline, acquiring the additional right-of-way for construction of the barrier, and maintaining access of water to residents in the area would far exceed the allowable CE threshold of \$21,000 benefited receptor.

### 5.2.13 Noise Area 13 – 85<sup>th</sup> Street South (Brett Avenue to Hughes Avenue)

Land use along the south side of 85<sup>th</sup> Street, from Brett Avenue to Hughes Avenue consists of residential receptors, consisting of multiple single family homes. The proposed project in this noise area will lower the profile along 85<sup>th</sup> Street approximately 2-3 feet and widen 85<sup>th</sup> Street to accommodate two through-lanes, right and left turn lanes.

Noise levels were modeled at 10 receptor locations in Noise Area 13. Modeled noise levels approached or exceeded the Federal NAC at 6 of 10 receptor locations with future (2045) Build conditions. For Receptor 13-4, the modeled noise level had a significant increase impact with future (2045) Build conditions. Noise abatement at this receptor was not feasible due to the need of direct access to the property off 85<sup>th</sup> Street. No mitigation was evaluated for this receptor.

#### 5.2.13.1 Barrier 13-1

An approximately 225 foot long, 9.2 foot high noise barrier was modeled on the south side of 85<sup>th</sup> Street, west of S Tuscan Club Circle, to mitigate impacts to the residential receptors 13-1 and 13-5. The barrier provides a reduction that varies from 1.7 to 7.0 dBA. Only one of the residences is benefited by the noise barrier, with a 7.0 dBA reduction, making the cost per benefited receptor is \$83,164, which exceeds the allowable CE threshold of \$21,000 benefited receptor.

#### 5.2.13.2 Barrier 13-2

An approximately 505 foot long, 20 foot high noise barrier was modeled on the south side of 85<sup>th</sup> Street, east of S Tuscan Club Circle, to mitigate impacts to the residential receptors 13-2, 13-3 and 13-7. The barrier provides a reduction that varies from 0.9 to 6.6 dBA. The noise barrier does not meet SDDOT's 7 dBA noise reduction design goal and is therefore not proposed.

## 5.2.14 Noise Area 14 – 85<sup>th</sup> Street South (Hughes Avenue to S Louise Avenue)

Land uses along the south side of 85<sup>th</sup> Street, from Hughes Avenue to S Louise Avenue consists of residential receptors, consisting of multiple single family homes and apartment complexes. The proposed project in this noise area will lower the profile approximately 1 foot in some areas along 85<sup>th</sup> Street. 85<sup>th</sup> Street will be widened to accommodate two through-lanes, right and left turn lanes at Hughes Avenue and signalized Hughes intersection.

Noise levels were modeled at 24 receptor locations in Noise Area 11. Modeled noise levels approached or exceeded the Federal NAC at 4 of 24 receptor locations with future (2045) Build conditions.

#### 5.2.14.1 Barrier 14-1

An approximately 445 foot long, 8.5 foot high noise barrier was modeled on the south side of 85<sup>th</sup> Street, east of Hughes Avenue, to mitigate impacts to the residential receptors 14-1 through 14-4. The barrier provides a reduction that varies from 0.9 to 7.5 dBA. 2 out of 4 (50%) of the benefited receptors achieve a noise reduction of 7.0 dBA or more. However, the cost per benefited receptor is \$41,363, which exceeds the allowable CE threshold of \$21,000 benefited receptor.

#### 5.2.15 Noise Area 15 – Northbound I-29 (East)

Land use east of I-29 Northbound consists of Sioux Fall Lutheran School, including various outdoor sports and recreational areas, which are located adjacent to the interstate. Closest receptors to the interstate represent a soccer field (Receptor 15-1) and track & field areas (receptors 15-2, 15-3 and 15-4). The school building itself is located further west from the interstate. The proposed project in this noise area constructs an auxiliary lane from 85<sup>th</sup> Street entrance ramp to I-229 northbound exit ramp at Louise Avenue, along the existing edge of pavement.

Noise levels were modeled at 4 receptor locations in Noise Area 15. Modeled noise levels approached or exceeded the Federal NAC at 1 of 4 receptor locations with future (2045) Build conditions.

#### 5.2.15.1 Barrier 15-1

An approximately 320 foot long, 20 foot high noise barrier was modeled on the west side of I-29 Northbound, to mitigate impacts to the exterior receptor 15-1. The barrier provides a reduction that varies from 0.6 to 3.6 dBA. The noise barrier does not meet SDDOT's 7 dBA noise reduction design goal and is therefore not proposed.

## 5.3 Previous Overpass EA Results

The previous Overpass EA analyzed eight noise areas for noise abatement based on the receptors surrounding the overpass construction limits, located along 270<sup>th</sup> Street and 85<sup>th</sup> Street. Abatement for seven of the noise areas were found to be either not feasible or not reasonable. Only one noise barrier, located along 85<sup>th</sup> Street, west to Beal Avenue, was determined to be reasonable and feasible. This noise barrier was modeled to mitigate impacts to the multi-family residential receptors at this location. The noise barrier was presented to the benefited residents and owners for voting as outlined in the SDDOT Noise Analysis and Abatement Guidance (effective date: July 13, 2011), as a part of the previous Overpass EA. More than 50% of the balloted voters were in favor of the construction of the noise barrier.

Barrier 9-3 was modeled to mitigate impacts to these same multi-family residential receptors along 85<sup>th</sup> Street at Beal Avenue for the proposed future (2045) Build conditions. Since this barrier was also determined to be reasonable and feasible, a new vote will be conducted for the benefited property owners and residents based on the barrier layout shown in Appendix C.

## 6 Construction Noise

The construction activities associated with implementation of the proposed project will result in increased noise levels relative to existing conditions. These impacts will primarily be associated with construction equipment and pile driving.

The following table (**Table 4**) shows peak noise levels monitored at 50 feet from various types of construction equipment. This equipment is primarily associated with site grading/site preparation, which is generally the roadway construction phase associated with the greatest noise levels.

Peak Noise Levels (dBA) **Manufacturers Total Number of Equipment Type** Sampled **Models in Sample** Range Average 74-92 **Backhoes** 5 6 83 Front Loaders 5 30 75-96 85 **Dozers** 8 41 65-95 85 72-92 Graders 3 15 84 2 27 87 Scrapers 76-98 Pile Drivers N/A N/A 95-105 101

Table 4 – Typical Construction Equipment Noise Levels at 50 Feet

Source: United States Environmental Protection Agency and Federal Highway Administration

Elevated noise levels are, to a degree, unavoidable for this type of project. SDDOT will require that contractors comply with the sound control requirements identified in the SDDOT Standard Specifications for Roads and Bridges. Construction noise abatement will be determined by weighing the duration of the project, benefits achieved, overall adverse social, economic and environmental effects, and cost of abatement measures.

It is anticipated that night construction may be required to minimize traffic impacts and to improve safety. However, construction will be limited to daytime hours as much as possible. If necessary, a detailed nighttime construction mitigation plan will be developed during the project final design stage.

Any associated high-impact equipment noise, such as pile driving, pavement sawing, or jack hammering, will be unavoidable with construction of the proposed project. Pile-driving noise is associated with any bridge construction and sheet piling necessary for retaining wall construction. High-impact noise construction activities will be limited in duration to the greatest extent possible. While pile-driving equipment results in the highest peak noise level, as shown in **Table 4**, it is limited in duration to the activities noted above (e.g., bridge construction). The use of pile drivers, jack hammers, and pavement sawing equipment will be prohibited during nighttime hours.

### 7 Conclusions

Noise levels surrounding the 85<sup>th</sup> Street project area exceed Federal NAC criteria for several single and multi-family receptors under the future build (2045) conditions, as well as at the outdoor soccer field at the Sioux Falls Lutheran School along I-29 Northbound.

In general, the construction of the I-29 interchange at 85<sup>th</sup> Street will result in increases in traffic noise levels compared to the existing conditions. Modeled build (2045) condition noise levels vary from 0.5 dBA to 20.7 dBA from existing (2015) conditions.

Generally, traffic noise levels are increased with the proposed build project due to many factors. Some of the major changes that influence the increases are as follows:

- Traffic demands will increase between the existing (2015) conditions and future (2045) conditions.
- The 85<sup>th</sup> Street corridor will be widened to two through-lanes, plus left and/or right turn lanes at various side roads along the corridor. The construction of additional lanes along 85<sup>th</sup> Street shifts the traffic closer to the existing receptors, resulting in increased noise levels.

Acoustic reasonableness and cost effectiveness were calculated for each of the 10 noise barriers that were evaluated for this study. One of the noise barriers (B9-3) was found to be reasonable and feasible and will follow the voting process for possible incorporation into this project, as outlined in the SDDOT Noise Analysis and Abatement Guidance (effective date: July 13, 2011).

If there are any significant changes to the final design of the I-29 and 85<sup>th</sup> Street Interchange project, the environmental document may need to be re-evaluated.

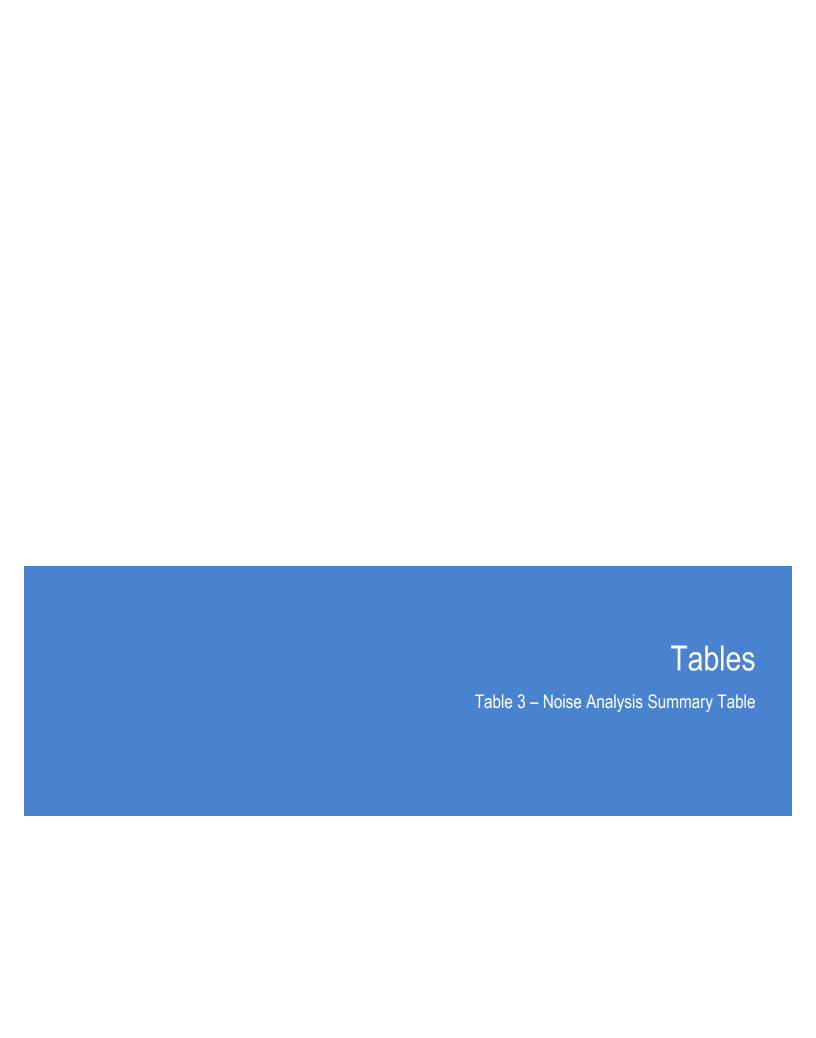


Table 3 Noise Analysis Summary Existing and Future Scenarios

Noise Level Comparison to Standards							
XX	<b>Bold</b> ; Approach or Exceeds FHWA Activity Criteria						
XX	Underline; substantial increase (15 dBA) in noise levels						
N/A	Receptor does not exist in Scenario						

\*Medical - Land Use is inpatient rehabilitation facility

Receiver					remanitation lacinty		
			Activity BA)	Existing Modeled 2015 Conditions	Future Build Conditions	Difference - Existing and Build	
		Activity	Criteria	L <sub>eq</sub>	L <sub>eq</sub>	$L_{eq}$	
<b>Receptor ID</b>		Category	$L_{eq}$	<b>⊢</b> eq	<b>⊏</b> eq	<b>⊢</b> eq	
Noise Area 1	& 2 - Sundowr	ner Ave					
1-1	Residential	В	67	46.7	57.4	10.7	
2-1	Residential	В	67	49.4	64.5	<u>15.1</u>	
2-2	Residential	В	67	47.9	54.1	6.2	
Noise Area 3	& 4 - South of	I-229 Northbo	ound				
3-1	Hospital	С	67	59.2	60.7	1.5	
3-2	Commercial	Е	72	56.6	58.5	1.9	
3-3	Medical*	С	67	61.8	63.3	1.5	
3-4	Medical*	С	67	58.0	59.6	1.6	
4-1	Commercial	E	72	65.0	66.7	1.7	
4-2	Commercial	E	72	58.4	59.6	1.2	
4-3	Commercial	E	72	60.2	60.7	0.5	
Noise Area 5	- 270th Street	(Between Elli	s Rd and Su	ndowner Ave)			
5-1	Residential	В	67	40.9	58.6	17.7	
5-2	Residential	В	67	40.2	49.8	9.6	
Noise Area 6	- Sundowner A	ve, North of	270th Street				
6-1	Residential	В	67	47.2	53.6	6.4	
6-2	Residential	В	67	47.1	54.1	7.0	
6-3	Residential	В	67	47.5	55.6	8.1	
				and Interchange)	33.3	<b>3</b>	
7-1	Residential	В	67	48.3	63.3	15.0	
7-2	Residential	В	67	49.0	65.8	16.8	
7-3	Residential	В	67	51.6	61.3	9.7	
7-4	Residential	В	67	48.2	N/A	0.1	
7-5	Residential	В	67	58.4	N/A		
	- 85th Street (I				14// (		
8-1	Residential	В	67	52.8	N/A		
8-2	Residential	В	67	49.0	69.0	20.0	
8-3	Residential	В	67	50.0	64.5	<u>20.0</u> 14.5	
8-4	Residential	В	67	50.9	69.1	18.2	
	- 85th Street (1				03.1	10.2	
9-1	Residential	B	67	49.8	64.3	14.5	
9-1		В		49.8 47.6	64.1		
9-2	Residential	В В	67 67	48.9	62.1	<u>16.5</u> 13.2	
9-3	Residential	В	67 67	47.4	63.9		
9-4	Residential	В	67	46.2	62.7	<u>16.5</u>	
9-5	Residential	В		46.8	63.4	<u>16.5</u>	
9-6	Residential	В	67 67		63.2	<u>16.6</u>	
	Residential	В	67 67	46.7		<u>16.5</u>	
9-8	Residential	В	67 67	47.0 50.5	63.8	<u>16.8</u>	
9-9A	Residential		67	50.5	70.4	<u>19.9</u>	
9-9B	Residential	В	67	50.3	70.6	20.3	
9-10	Residential	В	67	50.2	70.6	<u>20.4</u>	
9-11	Residential	В	67	50.1	70.4	<u>20.3</u>	

Table 3 Noise Analysis Summary Existing and Future Scenarios

Noise Level Comparison to Standards							
XX	<b>Bold</b> ; Approach or Exceeds FHWA Activity Criteria						
XX	Underline; substantial increase (15 dBA) in noise levels						
	Receptor does not exist in Scenario						

Receiver				Existing Modeled		
		FHWA Activity (dBA)		2015 Conditions	Future Build Conditions	Difference - Existing and Build
Receptor ID	Land Use	Activity Category	Criteria L <sub>eq</sub>	$L_{eq}$	$L_{eq}$	$L_{eq}$
	- 85th Street W			Ave)		
9-12	Residential	В	67	42.6	57.4	14.8
9-13	Residential	В	67	41.4	57.1	15.7
9-14	Residential	В	67	41.9	58.6	16.7
9-15	Residential	В	67	40.9	54.6	13.7
9-16	Residential	В	67	39.9	52.7	12.8
9-17	Residential	В	67	40.2	56.0	15.8
9-18	Residential	В	67	50.8	63.1	12.3
9-19	Residential	В	67	51.3	63.3	12.0
9-20	Residential	В	67	49.8	58.3	8.5
	0 - 85th Street	WB (Beal Ave				
10-1	Residential	В	67	48.2	67.6	19.4
10-2	Residential	В	67	48.3	66.8	18.5
10-3	Residential	В	67	49.3	68.1	18.8
10-4	Residential	В	67	48.5	66.9	18.4
10-5	Residential	В	67	48.8	67.3	18.5
10-6	Residential	В	67	48.6	67.0	18.4
10-7	Residential	В	67	48.7	66.8	18.1
10-8	Residential	В	67	48.9	67.1	18.2
10-9	Residential	В	67	48.8	66.8	18.0
10-10	Residential	В	67	49.0	66.9	17.9
10-11	Residential	В	67	50.2	68.3	18.1
10-12	Residential	В	67	49.1	65.7	16.6
10-13	Residential	В	67	51.9	68.9	17.0
10-14	Residential	В	67	43.7	59.0	15.3
10-15	Residential	В	67	43.0	57.3	14.3
10-16	Residential	В	67	43.5	57.5	14.0
10-17	Residential	В	67	43.5	57.5	14.0
10-18	Residential	В	67	43.6	57.4	13.8
10-19	Residential	В	67	43.6	57.4	13.8
10-20	Residential	В	67	43.7	57.5	13.8
10-21	Residential	В	67	43.9	57.5	13.6
10-22	Residential	В	67	44.0	57.5	13.5
10-23	Residential	В	67	45.5	59.1	13.6
10-24	Residential	В	67	44.4	57.7	13.3
10-25	Residential	В	67	48.2	62.6	14.4
10-26	Residential	В	67	46.0	58.9	12.9
10-27	Residential	В	67	44.9	57.4	12.5
10-28	Residential	В	67	45.8	64.0	<u>18.2</u>
10-29	Residential	В	67	43.9	61.3	<u>17.4</u>
10-30	Residential	В	67	42.6	58.4	<u>15.8</u>
10-31	Residential	В	67	42.5	57.1	14.6

Table 3 Noise Analysis Summary Existing and Future Scenarios

Noise Level Comparison to Standards							
XX	<b>Bold</b> ; Approach or Exceeds FHWA Activity Criteria						
XX Underline; substantial increase (15 dBA) in noise levels							
N/A	Receptor does not exist in Scenario						

Red	ceiver			Existing Modeled		
		FHWA Activity (dBA)		2015 Conditions	Future Build Conditions	Difference - Existing and Build
Receptor ID		Activity Category	Criteria L <sub>eq</sub>	L <sub>eq</sub>	L <sub>eq</sub>	$L_{eq}$
Noise Area 1	11 - 85th Street	WB (Hughes	Avenue to S	Louise Avenue)		
11-1	Residential	В	67	56.6	69.5	12.9
11-2	Residential	В	67	56.9	69.5	12.6
11-3	Residential	В	67	57.4	69.5	12.1
11-4	Residential	В	67	58.2	69.5	11.3
11-5	Residential	В	67	50.7	62.6	11.9
11-6	Residential	В	67	52.3	63.8	11.5
11-7	Residential	В	67	54.1	65.9	11.8
11-8	Residential	В	67	53.5	65.4	11.9
11-9	Residential	В	67	55.2	64.4	9.2
11-10	Residential	В	67	47.8	58.7	10.9
11-11	Residential	В	67	48.3	58.8	10.5
11-12	Residential	В	67	49.4	58.3	8.9
11-13	Residential	В	67	49.7	57.9	8.2
11-14	Residential	В	67	49.4	56.1	6.7
11-15	Residential	В	67	53.9	60.7	6.8
11-16	Residential	В	67	53.3	59.1	5.8
11-17	Residential	В	67	46.5	57.1	10.6
11-18	Residential	В	67	47.1	57.1	10.0
11-19	Residential	В	67	48.3	56.4	8.1
11-20	Residential	В	67	49.1	56.0	6.9
11-21	Residential	В	67	52.0	56.8	4.8
11-22	Residential	В	67	53.1	57.9	4.8
Noise Area 1	2 - 85th Street	EB (S Towns	ley Ave to S	Brett Ave)		
12-1	Residential	В	67	50.6	69.6	<u>19.0</u>
12-2	Residential	В	67	50.3	69.8	<u>19.5</u>
12-3	Residential	В	67	50.2	69.8	<u>19.6</u>
12-4	Residential	В	67	50.2	70.0	<u>19.8</u>
12-5	Residential	В	67	50.0	70.6	<u>20.6</u>
12-6	Residential	В	67	50.0	70.7	20.7
12-7	Residential	В	67	49.6	70.0	<u>20.4</u>
12-8	Residential	В	67	42.3	57.6	<u>15.3</u>
12-9	Residential	В	67	38.4	54.2	<u>15.8</u>
12-10	Residential	В	67	40.1	57.7	<u>17.6</u>
12-11	Residential	В	67	39.5	55.1	<u>15.6</u>
12-12	Residential	В	67	37.1	49.0	11.9
12-13	Residential	В	67	38.2	55.9	<u>17.7</u>
12-14	Residential	В	67	45.2	63.5	<u>18.3</u>
12-15	Residential	В	67	43.2	60.1	<u>16.9</u>
12-16	Residential	В	67	40.2	48.7	8.5
12-17	Residential	В	67	38.0	44.0	6.0
12-18	Residential	В	67	37.6	43.2	5.6
12-19	Residential	В	67	37.0	42.2	5.2

Table 3 Noise Analysis Summary Existing and Future Scenarios

	Noise Level Comparison to Standards										
XX	<b>Bold</b> ; Approach or Exceeds FHWA Activity Criteria										
XX	Underline; substantial increase (15 dBA) in noise levels										
N/A	Receptor does not exist in Scenario										

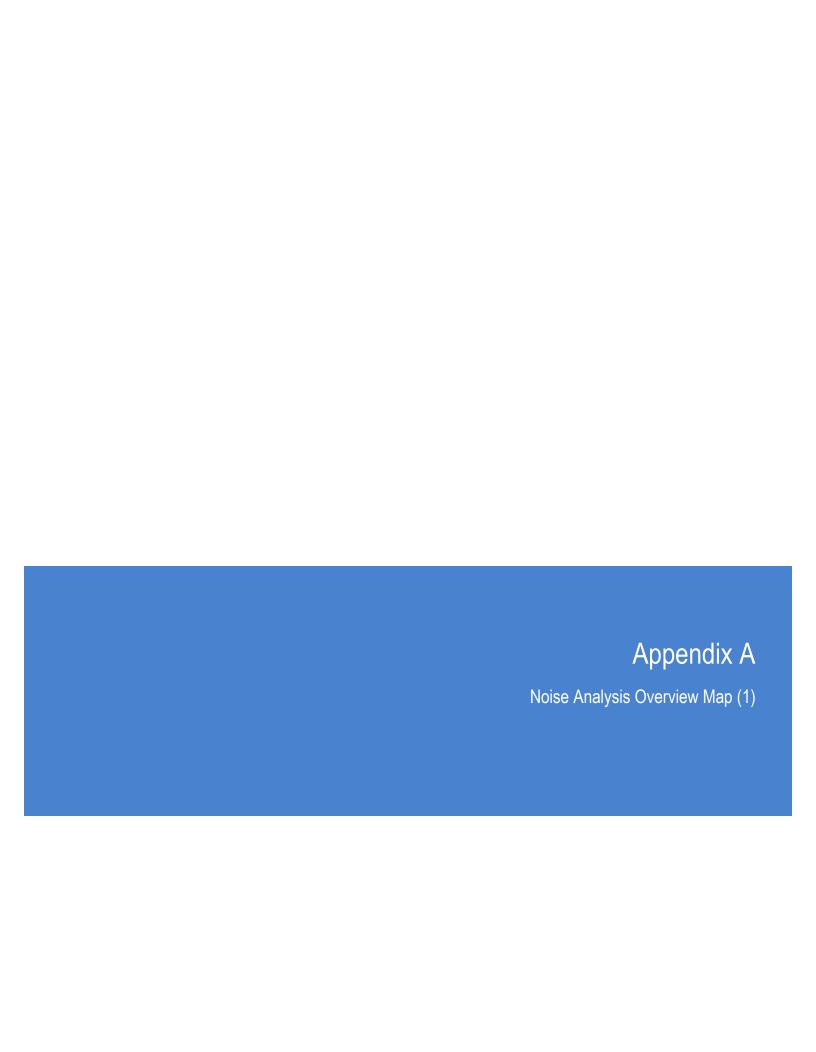
Red	ceiver			Existing Modeled		
		(dE		2015 Conditions	Future Build Conditions	Difference - Existing and Build
Receptor ID	Land Use	Activity Category	Criteria L <sub>ea</sub>	L <sub>eq</sub>	$L_{eq}$	$L_{eq}$
	2 - 85th Street			Brett Ave)		
12-20	Residential	В	67	37.2	42.0	4.8
12-21	Residential	В	67	37.4	47.0	9.6
12-22	Residential	В	67	43.3	56.2	12.9
12-23	Residential	В	67	40.2	52.8	12.6
12-24	Residential	В	67	38.3	48.7	10.4
12-25	Residential	В	67	38.0	47.8	9.8
12-26	Residential	В	67	37.9	48.1	10.2
12-27	Residential	В	67	38.1	49.4	11.3
12-28	Residential	В	67	41.5	55.5	14.0
12-29	Residential	В	67	41.3	54.5	13.2
	3 - 85th Street			•		
13-1	Residential	В	67	49.1	68.9	<u>19.8</u>
13-2	Residential	В	67	47.0	64.3	<u>17.3</u>
13-3	Residential	В	67	54.0	70.3	<u>16.3</u>
13-4	Residential	В	67	43.9	60.1	16.2
13-5	Residential	В	67	44.1	59.7	<u>15.6</u>
13-6 13-7	Residential	В	67	44.3 49.0	59.1 64.1	14.8
13-7	Residential Residential	B B	67 67	46.5	60.7	<u>15.1</u> 14.2
13-0	Residential	В	67	45.0	58.4	13.4
13-10	Residential	В	67	42.2	56.0	13.8
	4 - 85th Street	_			30.0	10.0
14-1	Residential	В	67	56.2	69.6	13.4
14-2	Residential	В	67	54.9	67.4	12.5
14-3	Residential	В	67	55.9	68.6	12.7
14-4	Residential	В	67	55.3	67.6	12.3
14-5	Residential	В	67	53.5	64.2	10.7
14-6	Residential	В	67	53.6	64.3	10.7
14-7	Residential	В	67	53.7	64.3	10.6
14-8	Residential	В	67	54.0	64.4	10.4
14-9	Residential	В	67	49.7	60.4	10.7
14-10	Residential	В	67	47.8	58.3	10.5
14-11	Residential	В	67	42.8	47.0	4.2
14-12	Residential	В	67	43.9	46.0	2.1
14-13	Residential	В	67	45.5	47.2	1.7
14-14	Residential	В	67	49.2	54.0	4.8
14-15	Residential	В	67	49.9	60.1	10.2
14-16	Residential	В	67 67	46.9	57.2	10.3
14-17	Residential	В	67 67	46.4 46.8	58.3 57.4	11.9
14-18	Residential	В	67	40.8	57.4	10.6

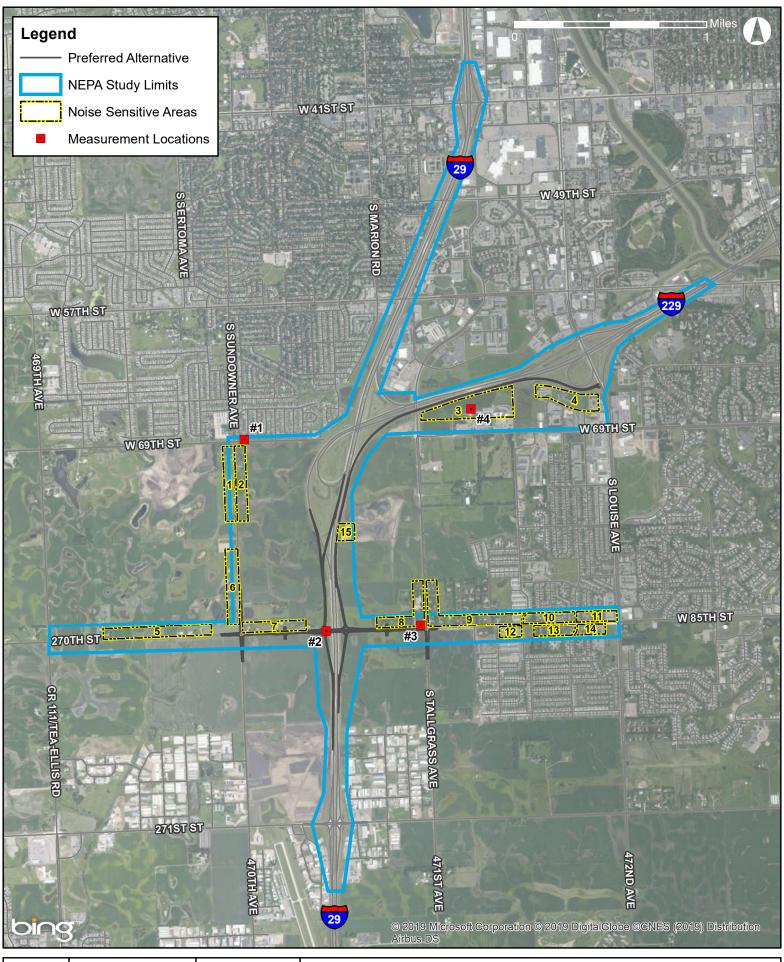
Table 3 Noise Analysis Summary Existing and Future Scenarios

	Noise Level Comparison to Standards										
XX	XX Bold; Approach or Exceeds FHWA Activity Criteria										
XX	<u>Underline</u> ; substantial increase (15 dBA) in noise levels										
N/A	Receptor does not exist in Scenario										

\*\*School - Land Use is outdoor school sports areas

Red	Receiver			Existing Modeled					
		FHWA /		2015 Conditions	Future Build Conditions	Difference - Existing and Build			
		Activity	Criteria		L <sub>eq</sub>				
Receptor ID	Land Use	Category	$L_{eq}$	Leq	<b>–</b> eq	Leq			
Noise Area 1	4 - 85th Street	EB (Hughes A	Ave to S Lou	ise Ave)					
14-19	Residential	В	67	46.5	56.2	9.7			
14-20	Residential	В	67	45.6	56.0	10.4			
14-21	Residential	В	67	44.8	50.9	6.1			
14-22	Residential	В	67	46.4	52.4	6.0			
14-23	Residential	В	67	47.9	53.9	6.0			
14-24	Residential	В	67	50.4	56.1	5.7			
Noise Area 1	5 - I-29 Northbo	ound (East)							
15-1	School**	С	67	68.2	70.3	2.1			
15-2	School**	С	67	62.0	64.0	2.0			
15-3	School**	C 67		62.6	64.7	2.1			
15-4	School**	С	67	62.7	64.9	2.2			





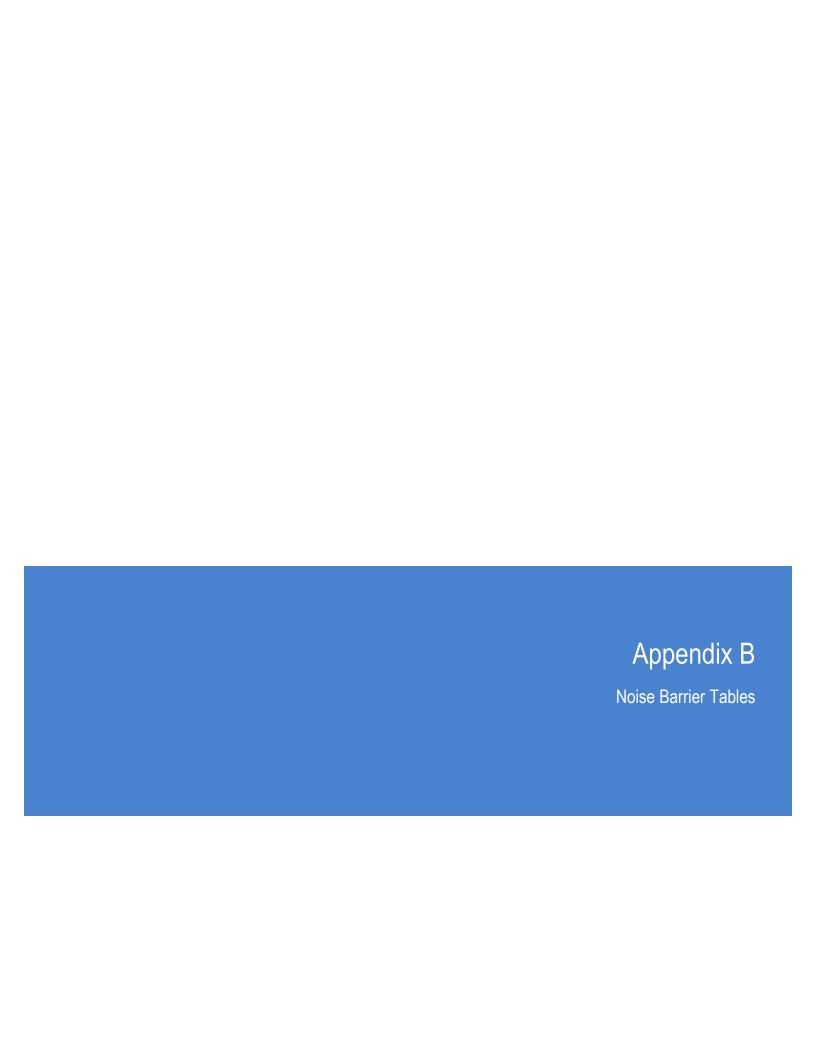


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Map by: mfalk Projection: State Plane South Dakota S

## **Noise Analysis Overview Map**

I-29 and 85th Street Interchange Lincoln County, SD



# Table B1 Build Noise Barrier Cost Effectiveness (Noise Area 9) Noise Barrier 9-1

			FHWA	Future No	ture Noise Levels Acoustic Effectiveness					Cost Effec	ctiveness (\$44/SF)			
Noise Barrier	Receiver	Land Use	Noise Standard (Leq dBA)	Build (Leq dBA)	Build with Barriers (Leq dBA)	dBA Reduction	Number of Receptors	Benefited Receptors (-5 dBA)	Barrier Length (ft)	Average Barrier Height (ft)	Area of Barrier (SF)	Total Cost	Cost per Benefited Receptor	NOISE WALL RESULTS
B9-1	9-3	Residential	67	62.1	61.4	-0.7	1	0	170	15	2550	\$112.200	N/A*	NO
D3-1	9-4	Residential	67	63.9	61.6	-23	1	0	170	13	2550	Ψ112,200	17/7	140

Number of Benefited Receptors (Front Row) = 0 (0%)

Total Number of Benefited Receptors = 0

Number of Receptors meeting Design Goal (7 dBA Reduction) = 0 (0%)

## Table B2 Build Noise Barrier Cost Effectiveness (Noise Area 9)

#### **Noise Barrier 9-2**

			FHWA	Future No	ise Levels	Acc	Acoustic Effectiveness			Cost Effec	ctiveness (\$44/SF)			
			Noise		Build with			Benefited					Cost per	NOISE
Noise			Standard	Build	Barriers	dBA	Number of	Receptors		Average Barrier			Benefited	WALL
Barrier	Receiver	Land Use	(Leq dBA)	(Leq dBA)	(Leq dBA)	Reduction	Receptors	(-5 dBA)	Barrier Length (ft)	Height (ft)	Area of Barrier (SF)	Total Cost	Receptor	RESULTS
B9-2	9-5	Residential	67	62.7	60.5	-2.2	1	0	180	16	2880	\$126,720	N/A*	NO
				Number of	of Benefited	Receptors (F	ront Row) =	0	(0%)					
				Total Number of Benefited Receptors =										

<sup>\*</sup>Design Goal and Acoustic Feasibility was not achieved since there are no Benefited Receptors

Number of Receptors meeting Design Goal (7 dBA Reduction) =

# Table B3 Build Noise Barrier Cost Effectiveness (Noise Area 9)

(0%)

Noise Barrier 9-3														
			FHWA	Future No	ise Levels	Acc	oustic Effective	ness		Cost Effec	ctiveness (\$44/SF)			
Noise Barrier	Receiver	Land Use	Noise Standard (Leq dBA)	Build (Leq dBA)	Build with Barriers (Leq dBA)	dBA Reduction	Number of Receptors	Benefited Receptors (-5 dBA)	Barrier Length (ft)	Average Barrier Height (ft)	Area of Barrier (SF)	Total Cost	Cost per Benefited Receptor	NOISE WALL RESULTS
	9-9A	Residential	67	70.4	66.5	-3.9	1	0						
	9-9B	Residential	67	70.6	62.9	-7.7	1	1						
	9-10	Residential	67	70.6	61.7	-8.9	2	2						
	9-11	Residential	67	70.4	62.0	-8.4	2	2						
B9-3	9-12	Residential	67	57.4	57.4	0.0	2	0	257	6	1542	\$67,848	\$13,570	YES
D9-3	9-13	Residential	67	57.1	57.1	0.0	4	0	231	U	1342	φ07,040	\$13,370	ILS
	9-14	Residential	67	58.6	58.6	0.0	2	0						
	9-15	Residential	67	54.6	54.6	0.0	2	0						
	9-16	Residential	67	52.7	52.7	0.0	4	0						
	9-17	Residential	67	56.0	55.8	-0.2	2	0						

Number of Benefited Receptors (Front Row) = 5 (83%)
Total Number of Benefited Receptors = 5
Number of Receptors meeting Design Goal (7 dBA Reduction) = 5 (100%)

Approx easements needed = 4785 SF Estimated Cost/SF = \$5 Cost / Benefited Receptor = \$4,785

TOTAL Cost / Benefited Receptor = \$18,355 (Includes Wall + Proposed Easements)

<sup>\*</sup>Design Goal and Acoustic Feasibility was not achieved since there are no Benefited Receptors

Table B4
Build Noise Barrier Cost Effectiveness (Noise Area 10)
Noise Barrier 10-1

			FHWA	Future No	ise Levels	Acoustic Effectiveness				Cos	t Effectivenes	s (\$44/SF)		
Noise Barrier	Receiver	Land Use	Noise Standard (Leq dBA)	Build (Leq dBA)	Build with Barriers (Leq dBA)	dBA Reduction	Number of Receptors	Benefited Receptors (-5 dBA)	Barrier Length (ft)	Average Barrier Height (ft)	Area of Barrier (SF)	Total Cost	Cost per Benefited Receptor	NOISE WALL RESULTS
	10-1	Residential	В	67.6	62.6	-5.0	1	1						
	10-2	Residential	В	66.8	59.2	-7.6	1	1						
	10-3	Residential	В	68.1	60.6	-7.5	1	1						
	10-4	Residential	В	66.9	60.4	-6.5	1	1						
	10-5	Residential	В	67.3	60.8	-6.5	1	1						
	10-6	Residential	В	67.0	60.2	-6.8	1	1						
	10-7	Residential	В	66.8	59.3	-7.5	1	1						
	10-8	Residential	В	67.1	59.3	-7.8	1	1						
	10-9	Residential	В	66.8	59.4	-7.4	1	1						
	10-10	Residential	В	66.9	59.2	-7.7	1	1						
	10-11	Residential	В	68.3	60.0	-8.3	1	1						
	10-12	Residential	В	65.7	59.3	-6.4	1	1						
	10-13	Residential	В	68.9	62.3	-6.6	1	1						
	10-14	Residential	В	59.0	55.3	-3.7	1	0						
	10-15	Residential	В	57.3	54.1	-3.2	1	0		_				
B10-1	10-16	Residential	В	57.5	54.5	-3.0	1	0	1387	6	8322	\$366,168	\$28,167	NO
	10-17	Residential	В	57.5	54.5	-3.0	1	0						
	10-18	Residential	В	57.4	54.4	-3.0	1	0						
	10-19	Residential	В	57.4	54.4	-3.0	1	0						
	10-20	Residential	В	57.5	54.3	-3.2	1	0						
	10-21	Residential	В	57.5	54.3	-3.2	1	0						
	10-22	Residential	В	57.5	54.4	-3.1	1	0						
	10-23	Residential	В	59.1	55.7	-3.4	1	0						
	10-24	Residential	В	57.7	54.2	-3.5	1	0						
	10-25	Residential	В	62.6	59.1	-3.5	1	0						
	10-26	Residential	В	58.9	56.3	-2.6	1	0						
	10-27	Residential	В	57.4	54.8	-2.6	1	0						
	10-28	Residential	В	64.0	60.1	-3.9	1	0						
	10-29	Residential	В	61.3	57.3	-4.0	1	0						
	10-30	Residential	B B	58.4	55.0 53.7	-3.4	1	0						
	10-31	Residential	В	57.1	53.7	-3.4		U						

Number of Benefited Receptors (Front Row) = 13 (100%)

Total Number of Benefited Receptors = 13

Number of Receptors meeting Design Goal (7 dBA Reduction) = 7 (54%)

Table B5
Build Noise Barrier Cost Effectiveness (Noise Area 10)
Noise Barrier 10-1 Alt 2

			FHWA	Future No	ise Levels		ustic Effectivene			Cos	t Effectiveness	s (\$44/SF)		
Noise Barrier	Receiver	Land Use	Noise Standard (Leq dBA)	Build (Leq dBA)	Build with Barriers (Leq dBA)	dBA Reduction	Number of Receptors	Benefited Receptors (-5 dBA)	Barrier Length (ft)	Average Barrier Height (ft)	Area of Barrier (SF)	Total Cost	Cost per Benefited Receptor	NOISE WALL RESULTS
	10-1	Residential	В	67.6	62.6	-5.0	1	1						
	10-2	Residential	В	66.8	59.3	-7.5	1	1						
	10-3	Residential	В	68.1	60.8	-7.3	1	1						
	10-4	Residential	В	66.9	61.0	-5.9	1	1						
	10-5	Residential	В	67.3	62.3	-5.0	1	1						
	10-6	Residential	В	67.0	61.8	-5.2	1	1						
	10-7	Residential	В	66.8	60.0	-6.8	1	1						
	10-8	Residential	В	67.1	60.0	-7.1	1	1						
	10-9	Residential	В	66.8	60.1	-6.7	1	1						
	10-10	Residential	В	66.9	59.8	-7.1	1	1						
	10-11	Residential	В	68.3	60.8	-7.5	1	1						
	10-12	Residential	В	65.7	59.8	-5.9	1	1						
	10-13	Residential	В	68.9	62.8	-6.1	1	1						
	10-14	Residential	В	59.0	55.3	-3.7	1	0						
	10-15	Residential	В	57.3	54.1	-3.2	1	0						
B10-1	10-16	Residential	В	57.5	54.9	-2.6	1	0	1387	5.4	7504	\$330,161	\$25,397	NO
	10-17	Residential	В	57.5	55.0	-2.5	1	0						
	10-18	Residential	В	57.4	55.0	-2.4	1	0						
	10-19	Residential	В	57.4	54.9	-2.5	1	0						
	10-20	Residential	В	57.5	54.8	-2.7	1	0						
	10-21	Residential	В	57.5	54.8	-2.7	1	0						
	10-22	Residential	В	57.5	54.9	-2.6	1	0						
	10-23	Residential	В	59.1	55.9	-3.2	1	0						
	10-24	Residential	В	57.7	54.4	-3.3	1	0						
	10-25	Residential	В	62.6	59.4	-3.2	1	0						
	10-26	Residential	В	58.9	56.5	-2.4	1	0						
	10-27	Residential	В	57.4	54.9	-2.5	1	0						
	10-28	Residential	В	64.0	60.1	-3.9	1	0						
	10-29	Residential	В	61.3	57.3	-4.0	1	0						
	10-30	Residential	В	58.4	55.0	-3.4	1	0						
	10-31	Residential	В	57.1	53.7	-3.4	1	0						

Number of Benefited Receptors (Front Row) = 13 (100%)

Total Number of Benefited Receptors = 13

Number of Receptors meeting Design Goal (7 dBA Reduction) = 5 (38%)

Table B6
Build Noise Barrier Cost Effectiveness (Noise Area 11)
Noise Barrier 11-1

			FHWA	Future No	ise Levels	Acou	stic Effective	eness		Cost Et	fectivene	ss (\$44/SF)		
Noise Barrier	Receiver	Land Use	Noise Standard (Leq dBA)	Build (Leq dBA)	Build with Barriers (Leq dBA)	dBA Reduction	Number of Receptors	Benefited Receptors (-5 dBA)	Barrier Length (ft)	Average Barrier Height (ft)	Area of Barrier (SF)	Total Cost	Cost per Benefited Receptor	NOISE WALL RESULTS
	11-1	Residential	67	69.5	64.4	-5.1	1	1						
	11-2	Residential	67	69.5	63.6	-5.9	1	1						
	11-3	Residential	67	69.5	61.8	-7.7	1	1						
	11-4	Residential	67	69.5	62.5	-7.0	1	1						
	11-5	Residential	67	62.6	60.0	-2.6	1	0						
	11-6	Residential	67	63.8	59.5	-4.3	1	0						
	11-7	Residential	67	65.9	59.7	-6.2	1	1						
	11-8	Residential	67	65.4	58.4	-7.0	1	1						
	11-9	Residential	67	64.4	62.0	-2.4	1	0						
	11-10	Residential	67	58.7	56.9	-1.8	1	0						
B11-1	11-11	Residential	67	58.8	56.7	-2.1	1	0	745	6.4	4746	\$208,809	\$34,801	NO
D11-1	11-12	Residential	67	58.3	55.3	-3.0	1	0	745	0.4	4740	Ψ200,009	ψ54,001	INO
	11-13	Residential	67	57.9	55.1	-2.8	1	0						
	11-14	Residential	67	56.1	54.1	-2.0	1	0						
	11-15	Residential	67	60.7	60.0	-0.7	1	0						
	11-16	Residential	67	59.1	58.6	-0.5	1	0						
	11-17	Residential	67	57.1	55.6	-1.5	1	0						
	11-18	Residential	67	57.1	55.2	-1.9	1	0						
	11-19	Residential	67	56.4	54.1	-2.3	1	0						
	11-20	Residential	67	56.0	53.8	-2.2	1	0						
	11-21	Residential	67	56.8	56.1	-0.7	1	0						
	11-22	Residential	67	57.9	57.5	-0.4	1	0						

Number of Benefited Receptors (Front Row) = 4 (100%)

Total Number of Benefited Receptors = 6

Number of Receptors meeting Design Goal (7 dBA Reduction) = 3 (50%)

Table B7
Build Noise Barrier Cost Effectiveness (Noise Area 11)
Noise Barrier 11-1 Alt 2

FHWA Future Noise Levels Acoustic Effectiveness Cost Effectiveness (\$44/SF)												1		
			FHWA	Future No		Acou	istic Effective					ss (\$44/SF)	Coot nor	1
			Noise	Build	Build with Barriers	dBA	Number of	Benefited Receptors	Barrier	Average Barrier	Area of Barrier		Cost per Benefited	NOISE
Noise Barrier	Receiver	Land Use	Standard (Leq dBA)	(Leq dBA)	(Leq dBA)	Reduction	Receptors	(-5 dBA)	Length (ft)	Height (ft)	(SF)	Total Cost	Receptor	WALL RESULTS
barrier			,				. 1000 p 10.0	( 0 427.1)	==::9::: ()		(0.)		. 1000/2101	RESULTS
	11-1	Residential	67	69.5	64.4	-5.1	1	1						
	11-2	Residential	67	69.5	64.3	-5.2	1	1						
	11-3	Residential	67	69.5	62.5	-7.0	1	1						
	11-4	Residential	67	69.5	63.6	-5.9	1	1						
	11-5	Residential	67	62.6	60.1	-2.5	1	0						
	11-6	Residential	67	63.8	59.7	-4.1	1	0						
	11-7	Residential	67	65.9	60.7	-5.2	1	1						
	11-8	Residential	67	65.4	59.0	-6.4	1	1						
	11-9	Residential	67	64.4	62.2	-2.2	1	0						
	11-10	Residential	67	58.7	57.0	-1.7	1	0						
B11-1	11-11	Residential	67	58.8	56.8	-2.0	1	0	745	5.7	4224	\$185,863	\$30,977	NO
D11-1	11-12	Residential	67	58.3	55.6	-2.7	1	0	745	5.1	4224	φ105,005	φ30,911	INO
	11-13	Residential	67	57.9	55.4	-2.5	1	0						
	11-14	Residential	67	56.1	54.4	-1.7	1	0						
	11-15	Residential	67	60.7	60.1	-0.6	1	0						
	11-16	Residential	67	59.1	58.6	-0.5	1	0						
	11-17	Residential	67	57.1	55.6	-1.5	1	0						
	11-18	Residential	67	57.1	55.3	-1.8	1	0						
	11-19	Residential	67	56.4	54.3	-2.1	1	0						
	11-20	Residential	67	56.0	54.1	-1.9	1	0						
	11-21	Residential	67	56.8	56.1	-0.7	1	0						
	11-22	Residential	67	57.9	57.5	-0.4	1	0						

Number of Benefited Receptors (Front Row) = 3 (75%)

Total Number of Benefited Receptors = 6

Number of Receptors meeting Design Goal (7 dBA Reduction) = 1 (17%)

Table B8
Build Noise Barrier Cost Effectiveness (Noise Area 12)
Noise Barrier 12-1

	1	1	1				ise Dairie							1
			FHWA	Future No	ise Levels	Acou	ıstic Effective				Effectiveness (\$4	4/SF)		
			Noise		Build with			Benefited		Average			Cost per	NOISE
Noise			Standard	Build	Barriers	dBA	Number of		Barrier	Barrier	Area of Barrier		Benefited	WALL
Barrier	Receiver	Land Use		(Leq dBA)	(Leq dBA)	Reduction	Receptors	(-5 dBA)	Length (ft)	Height (ft)	(SF)	Total Cost	Receptor	RESULTS
	12-1	Residential	67	69.6	61.0	-8.6	3	3						
	12-2	Residential	67	69.8	60.6	-9.2	2	2						
	12-3	Residential	67	69.8	61.0	-8.8	2	2						
	12-4	Residential	67	70.0	61.4	-8.6	2	2						
	12-5	Residential	67	70.6	62.4	-8.2	2	2						
	12-6	Residential	67	70.7	63.3	-7.4	3	3						
	12-7	Residential	67	70.0	63.4	-6.6	1	1						
	12-8	Residential	67	57.6	57.5	-0.1	3	0						
	12-9	Residential	67	54.2	54.0	-0.2	2	0						
	12-10	Residential	67	57.7	53.7	-4.0	2	0						
	12-11	Residential	67	55.1	51.6	-3.5	2	0						
	12-12	Residential	67	49.0	49.0	0.0	2	0						
	12-13	Residential	67	55.9	51.1	-4.8	3	0						
	12-14	Residential	67	63.5	62.4	-1.1	1	0						
B12-1	12-15	Residential	67	60.1	59.4	-0.7	2	0	650	6	3900	\$171,600	\$11,440	YES *
	12-16	Residential	67	48.7	48.7	0.0	3	0						
	12-17	Residential	67	44.0	44.0	0.0	2	0						
	12-18	Residential	67	43.2	43.3	0.1	2	0						
	12-19	Residential	67	42.2	42.2	0.0	2	0						
	12-20	Residential	67	42.0	42.1	0.1	2	0						
	12-21	Residential	67	47.0	47.0	0.0	3	0						
	12-22	Residential	67	56.2	55.7	-0.5	2	0						
	12-23	Residential	67	52.8	52.8	0.0	2	0						
	12-24	Residential	67	48.7	48.8	0.1	3	0						
	12-25	Residential	67	47.8	47.8	0.0	2	0						
	12-26	Residential	67	48.1	48.1	0.0	2	0						
	12-27	Residential	67	49.4	49.5	0.1	3	0						
	12-28	Residential	67	55.5	55.2	-0.3	1	0						
	12-29	Residential	67	54.5	54.2	-0.3	2	0						

Number of Benefited Receptors (Front Row) = 15 (100%)

Total Number of Benefited Receptors = 15

Number of Receptors meeting Design Goal (7 dBA Reduction) = 14 (93%)

<sup>\*</sup> Barrier is not feasible to construct due to Lewis & Clark Water utility, which cannot be impacted or relocated.

Table B9
Build Noise Barrier Cost Effectiveness (Noise Area 13)
Noise Barrier 13-1

			FHWA	Future No	ise Levels	Acou	ustic Effective	ness		Cost Effe	ctiveness	(\$44/SF)		
			Noise	Build	Build with Barriers	dBA	Number of	Benefited Receptors	Barrier	Average Barrier	Area of Barrier		Cost per Benefited	NOISE
Noise Barrier	Receiver	Land Use	Standard (Leq dBA)			Reduction	Receptors	(-5 dBA)				Total Cost	Receptor	WALL RESULTS
B13-1	13-1	Residential	67	68.9	61.9	-7.0	1	1	205	9.2	1890.1	\$83,164	\$83,164	NO
D13-1	13-5	Residential	67	59.7	58.0	-1.7	1	0	205	9.2	1090.1	ФОЗ, 104	ФОЗ, 104	NO
			Number of Benefited Receptors (Front Row) =					1	(100%)					

Number of Benefited Receptors (Front Row) = 1 (100%)

Total Number of Benefited Receptors = 1

Number of Receptors meeting Design Goal (7 dBA Reduction) = 1 (100%)

Table B10
Build Noise Barrier Cost Effectiveness (Noise Area 13)
Noise Barrier 13-2

			FHWA	Future No	ise Levels	Acou	ustic Effective	eness		Cost Effe	ctiveness	(\$44/SF)		
Noise Barrier	Receiver	Land Use	Noise Standard (Leq dBA)	Build (Leq dBA)	Build with Barriers (Leq dBA)	dBA Reduction	Number of Receptors	Benefited Receptors (-5 dBA)	Barrier Length (ft)	Average Barrier Height (ft)	Area of Barrier (SF)	Total Cost	Cost per Benefited Receptor	NOISE WALL RESULTS
	13-2	Residential	67	64.3	59.0	-5.3	1	1						
	13-3	Residential	67	70.3	63.7	-6.6	1	1						
B13-2	13-6	Residential	67	59.1	56.3	-2.8	1	0	505	18.0	9090	\$399,960	\$99,990	NO
D13-2	13-7	Residential	67	64.1	58.3	-5.8	1	1	303	10.0	9090	ψυσσ,σου	ψ99,990	NO
	13-8	Residential	67	60.7	55.7	-5.0	1	1						
	13-9	Residential	67	58.4	54.0	-4.4	1	0						

Number of Benefited Receptors (Front Row) = 2 (100%)

Total Number of Benefited Receptors = 4

Number of Receptors meeting Design Goal (7 dBA Reduction) = 0 (0%)

Table B11
Build Noise Barrier Cost Effectiveness (Noise Area 14)
Noise Barrier 14-1

			FHWA	Future No	ise Levels	Aco	ustic Effective	eness		Cost Effec	tiveness (\$	44/SF)		
Noise Barrier	Receiver	Land Use	Noise Standard (Leq dBA)	Build (Leq dBA)	Build with Barriers (Leq dBA)	dBA Reduction	Number of Receptors	Benefited Receptors (-5 dBA)	Barrier Length (ft)	Average Barrier Height (ft)	Area of Barrier (SF)	Total Cost	Cost per Benefited Receptor	NOISE WALL RESULTS
	14-1	Residential	67	69.6	63.8	-5.8	1	1						
	14-2	Residential	67	67.4	60.9	-6.5	1	1						
	14-3	Residential	67	68.6	61.1	-7.5	1	1						
	14-4	Residential	67	67.6	60.6	-7.0	1	1						
	14-9	Residential	67	60.4	57.8	-2.6	1	0						
B14-1	14-10	Residential	67	58.3	55.5	-2.8	1	0	445	8.5	3760	\$165,451	\$41,363	NO
D14-1	14-15	Residential	67	60.1	57.3	-2.8	1	0	440	0.5	3700	ψ100,401	ψ41,505	INO
	14-16	Residential	67	57.2	54.5	-2.7	1	0						
	14-17	Residential	67	58.3	57.4	-0.9	1	0						
	14-18	Residential	67	57.4	55.7	-1.7	1	0						
	14-19	Residential	67	56.2	53.9	-2.3	1	0						
	14-20	Residential	67	56.0	53.3	-2.7	1	0						

Number of Benefited Receptors (Front Row) = 4 (100%)

Total Number of Benefited Receptors = 4

Number of Receptors meeting Design Goal (7 dBA Reduction) = 2 (50%)

Table B12
Build Noise Barrier Cost Effectiveness (Noise Area 15)
Noise Barrier 15-1

			FHWA	Future No	ise Levels	Acou	ıstic Effective	ness		Cost Effe	ectivenes	s (\$44/SF)		
			Noise		Build with			Benefited		Average	Area of		Cost per	NOISE
Noise			Standard	Build (Leg dBA)	Barriers (Leq dBA)	dBA Reduction	Number of Receptors	Receptors (-5 dBA)	Barrier Length (ft)	Barrier Height (ft)	Barrier (SF)	Total Cost	Benefited Receptor	WALL
Barrier	Receiver	Land Use	(Leq dBA)	(Leq ubA)	(Leq ubA)	Reduction	Receptors	(-3 dbA)	Lengin (it)	rieigni (ii)	(31)	Total Cost	Receptor	RESULTS
	15-1	School	67	70.3	66.7	-3.6	1	0						
B15-1	15-2	School	67	64.0	62.6	-1.4	1	0	320	20	6400	\$281,600	N/A*	NO
D13-1	15-3	School	67	64.7	63	-1.7	1	0	320	20	0400	φ201,000	IN/A	INO
	15-4	School	67	64.9	64.3	-0.6	1	0						

Number of Benefited Receptors (Front Row) = 0 (100%)

Total Number of Benefited Receptors = 0

Number of Receptors meeting Design Goal (7 dBA Reduction) = 0 (0%)

<sup>\*</sup>Design Goal and Acoustic Feasibility was not achieved since there are no Benefited Receptors







Print Date: 1/2/2020 Source: Bing Maps, Lincoln County

Noise Analysis Future Build Results and Barrier Locations: NSA's 1, 2 and 6 I-29 and 85th Street Interchange Lincoln County, SD Map by: mfalk Projection: State Plane South Dakota S



350 525 700





Print Date: 1/22/2020 Source: Bing Maps, Lincoln County

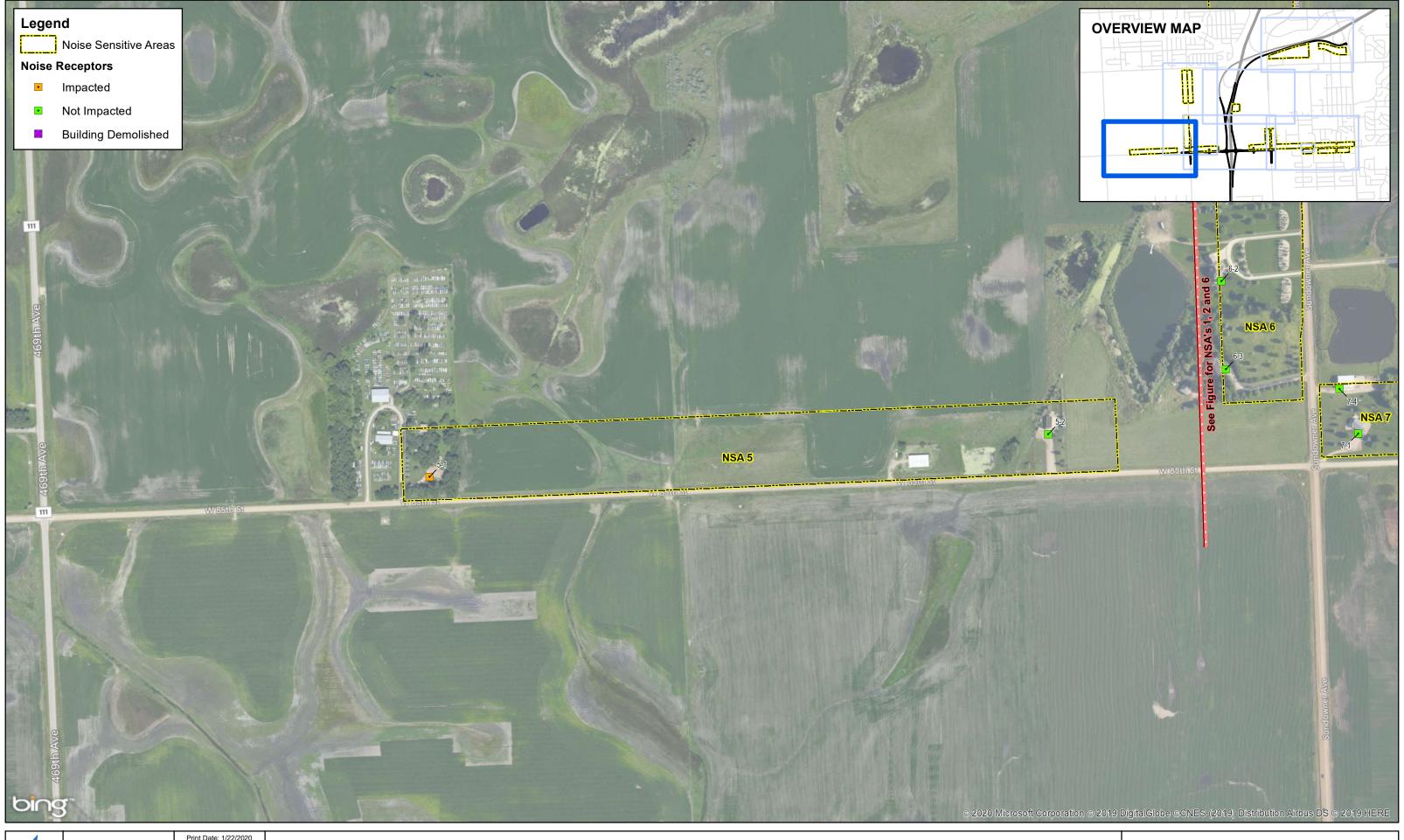
Map by: mfalk
Projection: State Plane
South Dakota S

Noise Analysis Future Build Results and Barrier Locations: NSA's 3 and 4

I-29 and 85th Street Interchange

Lincoln County, SD

Feet 175 350 525 700





Print Date: 1/22/2020 Source: Bing Maps, Lincoln County

Map by: mfalk Projection: State Plane South Dakota S I-29 and 85th Street Interchange Lincoln County, SD





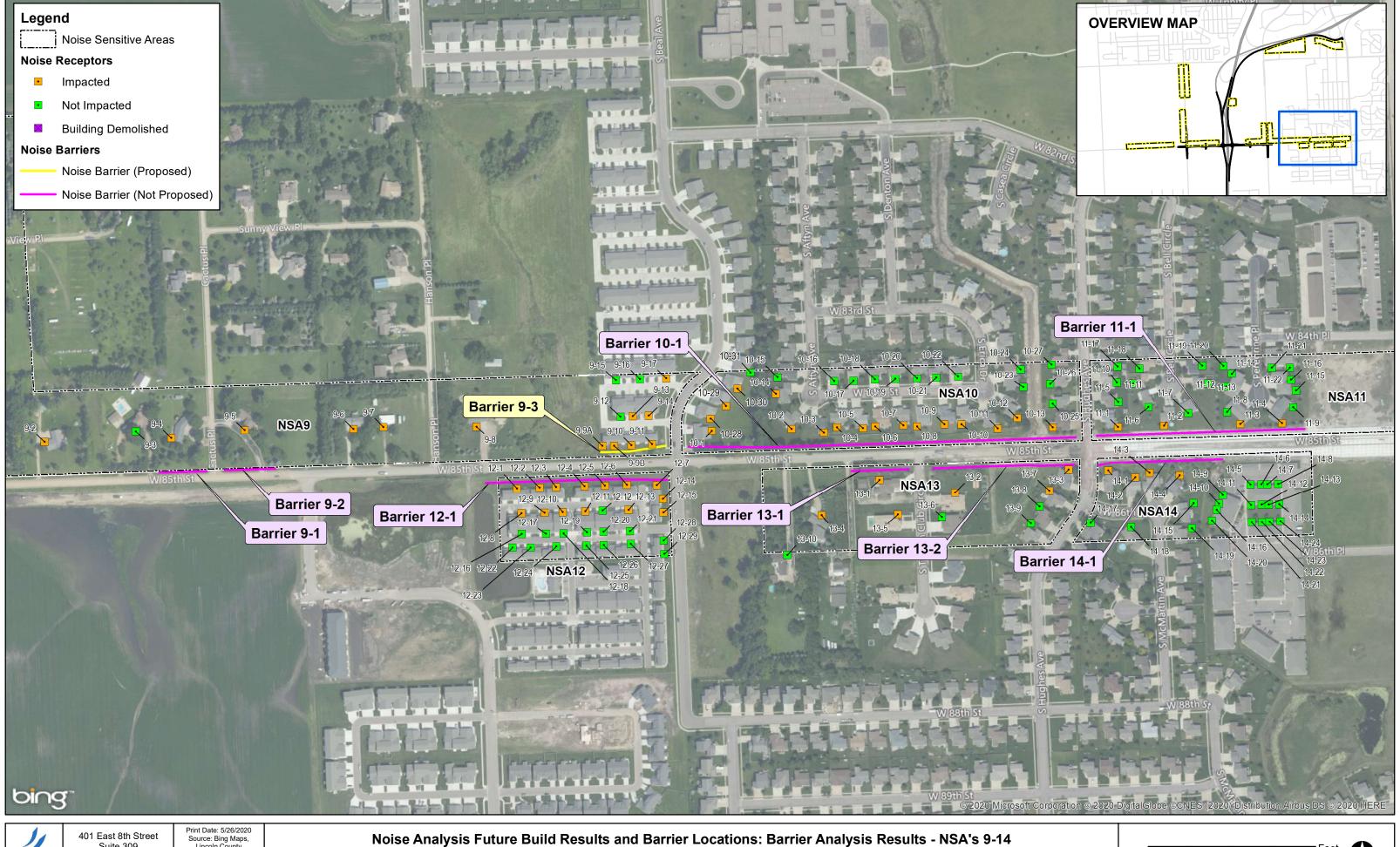


Print Date: 1/22/2020 Source: Bing Maps, Lincoln County

Map by: mfalk
Projection: State Plane
South Dakota S

Noise Analysis Future Build Results and Barrier Locations: NSA's 7 and 8

I-29 and 85th Street Interchange
Lincoln County, SD





Suite 309 Sioux Falls, SD 57103 (605) 330-7000

Print Date: 5/26/2020 Source: Bing Maps, Lincoln County

Map by: mfalk Projection: State Plane South Dakota S

I-29 and 85th Street Interchange Lincoln County, SD





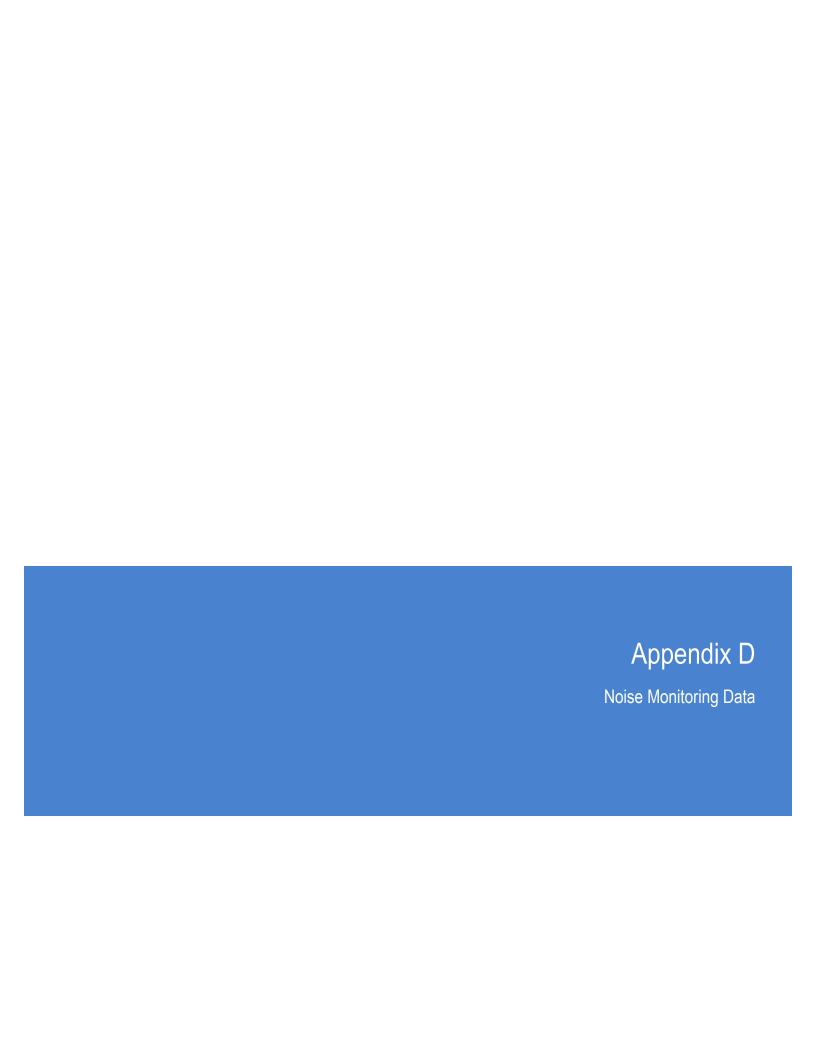
Suite 309 Sioux Falls, SD 57103 (605) 330-7000

Print Date: 1/22/2020 Source: Bing Maps, Lincoln County

Map by: mfalk Projection: State Plane South Dakota S

Noise Analysis Future Build Results and Barrier Locations: Barrier Analysis Results - NSA 15 I-29 and 85th Street Interchange Lincoln County, SD

100 200 400 300



Monitor Location 1: File Name on Meter 831 Data.007 North of 69th St, East of Sundowner Ave File Name on PC SLM\_0004132\_831\_Data\_007.00.ldbin Coords: Serial Number 0004132 Model Model 831 43° 29' 24.5"N 096° 48' 18.7"W Firmware Version 2.314 Traffic (Cars/MT/HT estimated hourly from short count): EB - 4 / 0 / 0 Location WB-4/0/0 Job Description 85th Street Interchange Project Note Measurem Description 2019-07-02 10:10:02 Stop 2019-07-02 10:40:04 00:30:02.5 . Duration Run Time 00:30:02.5 00:00:00.0 Pre Calibration 2019-07-02 10:06:44 Post Calibration None Calibration Deviation Overall Settings RMS Weight A Weighting Peak Weight A Weighting Detector PRM831 Preamp Microphone Correction Off Integration Method Linear 0.0 dB Gain Overload 145.2 dB Α С Under Range Peak 77.8 74.8 79.8 dB 27.6 27.0 **Under Range Limit** 33.8 dB Noise Floor 17.8 18.4 24.1 dB LAeq 53.9 LAE EA 86.5 49.152 μPa²h 2019-07-02 10:34:22 96 7 dB I Aneak (may LAFmax 2019-07-02 10:34:23 83.6 dB LAFmin 2019-07-02 10:37:38 37.6 dB SEA LAF > 65.0 dB (Exceedance Counts / Duration) 21.1 s LAF > 85.0 dB (Exceedance Counts / Duration) 0 0.0 s LApeak > 135.0 dB (Exceedance Counts / Duration) 0 0.0 s LApeak > 137.0 dB (Exceedance Counts / Duration) 0.0 s LApeak > 140.0 dB (Exceedance Counts / Duration) 0 0.0 s **Community Noise** Ldn LDay 07:00-23:00 LNight 23:00-07:00 LDay 07:00-19:00 LEvening 19:00-23:00 LNight 23:00-07:00 53.9 53.9 53.9 LCeq 63.5 dB LAeq LCeq - LAeq 53.9 dB 9.6 dB LAleq 57.0 dB LAea 53.9 dB LAleq - LAeq 3.1 dB A dB C Time Stamp Time Stamp dB Time Stamp Leq 53.9 63.5 67.5 88.6 2019/07/02 10:34:23 89.7 2019/07/02 10:34:23 80.9 2019/07/02 10:34:23 LS(max) 83.6 2019/07/02 10:34:23 91.4 2019/07/02 10:34:23 92.7 2019/07/02 10:34:23 LF(max) LI(max) 84.4 39.0 2019/07/02 10:34:23 2019/07/02 10:31:45 92.6 2019/07/02 10:34:23 94.0 2019/07/02 10:34:23 55.4 2019/07/02 10:23:20 LS(min) 52.6 2019/07/02 10:32:47 37.6 2019/07/02 10:37:38 50.5 2019/07/02 10:32:46 53.7 2019/07/02 10:19:08 LF(min) LI(min) 38.5 2019/07/02 10:32:23 53.3 2019/07/02 10:32:44 56.2 2019/07/02 10:23:18 101.1 2019/07/02 10:34:23 102.5 2019/07/02 10:34:23 96.7 2019/07/02 10:34:22 LPeak(max) 0 # Overloads Overload Duration 0.0 s LAI5.00 54.4 dB LAI10.00 51.7 dB LAI33.30 45.4 dB LAI50.00 43.8 dB LAI66.60 42.9 dB LAI90.00 41.0 dB Calibration Histor dB re. 1V/Pa 10.0 Preamp Date 6.3 8.0 12.5 PRM831 2019-07-02 10:06:39 -27.8 46.5 45.9 42.4 44.4 PRM831 2019-07-02 09:03:47 -27.8 58.2 64.9 63.3 60.1 PRM831 2019-06-13 09:39:04 -27.8 69.7 55.0 61.1 PRM831 2019-06-06 09:54:09 -27.8 54 5 56.4 64 1 69 3 PRM831 2019-06-06 09:53:46 -27.8 50.2 48.1 52.6 50.2 PRM831 2019-06-05 19:18:32 2019-06-05 19:13:22 -27.7 58.2 56.4 51.0 60.3 -27.7 55.2 PRM831 53.0 54.7 52.1 PRM831 2019-06-05 11:53:15 -27.9 63.3 57.9 60.0 58.9 PRM831 2019-04-18 13:26:43 -27.8 60.1 51.2 50.0 64.6 PRM831 2019-03-22 11:28:03 -27.6 27.7 50.3 137.6 72.3 PRM831 2019-03-22 11:01:16 -26.0

I-29 / 85th St (noi				nl	tos Taken; Yes/No	
Dat Locatio	e: $7-2-19$	t of Sundowner; nort of 6	9th)		on of Unit: Yes/No	
GPS Coordinate	es: $43.4901$	40 (N) 96.80519 (W)	, ,	Canbrut	Weather: 760	
Start tim		, (1) / (1)				cloudy
Finish tim	e: 10:40 am				wind	5-bmph (N)
	831_Bata	$\phi\phi$ 7			00 (0-0)	) owepre de
	Vehicle Count					Total
senger	wb	11				2
passenger	eb	11				2
·unit						
single-unit truck						
snq						
truck avy ick						
semi truck / heavy truck						
	Tota	ı				4
Site Set-up Diagra	am		Noise Comr	ments		
A Note of the second se	n //		- AC c	units running in house writer monitoring monitoring bam-water truck on and am-	es north of	setup
3		Mackenzie	- 1¢:1¢	bam-water truck on !	sendowner (ba	ckup beeper
Scadowne		Macket	10,17	(1		((
2c n			-14.17	am		
1	~		- (Φ', 3(	am-airplane		
3	69th St.		-			
Oga 6	0/- 11.	(Grave)				
	* talked to	o homeowner and she had no	issue			

 $\label{thm:linear_continuous_continuous_continuous} \label{thm:linear_continuous_conti$ 



Site M1: 69<sup>th</sup> Street, east of Sundowner Avenue Camera Facing South (07/02/2019)

Summary File Name on Meter 831 Data.008

File Name on PC SLM\_0004132\_831\_Data\_008.00.ldbin Serial Number 0004132 Model Model 831

Firmware Version Justin Anibas

Location

Job Description 85th Street Interchange Project Note

Monitor Location 2:

East end of 85th St near I-29 Southbound

43° 28' 31.7"N 096° 47' 51.4"W

Traffic (Cars/MT/HT estimated hourly from short count):

NB - 1276 / 32 / 184 SB - 1046 / 28 / 154

Measurement Description

2019-07-02 11:02:27 Start 2019-07-02 11:32:58 Stop Duration Run Time 00:30:31.0 00:00:00.0 Pause

Pre Calibration 2019-07-02 10:55:46 Post Calibration None **Calibration Deviation** 

Overall Settings RMS Weight

A Weighting Peak Weight A Weighting Detector Fast PRM831 Preamp Microphone Correction Off Linear Integration Method 0.0 dB Gain Overload 145.1 dB

A 77.7 **C** 74.7 **z** 79.7 dB Under Range Peak Under Range Limit 27.0 27.5 33.7 dB Noise Floor 17.8 18.4 24.0 dB

2.314

Results LAeq

64.6 LAE 97.2 EΑ 582.407 μPa<sup>2</sup>h

2019-07-02 11:31:26 LApeak (max) 92.9 dB LAFmax 2019-07-02 11:11:19 77.7 dB LAFmin 2019-07-02 11:19:15 48.6 dB

SEA 99.9 dB

LAF > 65.0 dB (Exceedance Counts / Duration) 100 624.7 s LAF > 85.0 dB (Exceedance Counts / Duration) LApeak > 135.0 dB (Exceedance Counts / Duration) 0.0 s 0.0 s 0 LApeak > 137.0 dB (Exceedance Counts / Duration) 0 0.0 s LApeak > 140.0 dB (Exceedance Counts / Duration) 0 0.0 s

**Community Noise** Ldn LDay 07:00-23:00 LNight 23:00-07:00 LDay 07:00-19:00 LEvening 19:00-23:00 64.6 64.6 64.6

LCeq 75.0 dB LAeq LCeq - LAeq 64.6 dB 10.4 dB LAleq 65.8 dB LAeq 64.6 dB LAleq - LAeq 1.2 dB

LS(max) LF(max) LI(max) LS(min) LF(min) LI(min)

LPeak(max)

A			C		4
dB	Time Stamp	dB	Time Stamp	dB	Time Stamp
64.6		75.0		76.5	
75.7	2019/07/02 11:31:27	90.0	2019/07/02 11:10:06	90.4	2019/07/02 11:10:06
77.7	2019/07/02 11:11:19	90.9	2019/07/02 11:10:06	91.3	2019/07/02 11:10:06
78.5	2019/07/02 11:11:19	91.4	2019/07/02 11:10:06	91.8	2019/07/02 11:10:06
50.3	2019/07/02 11:19:15	61.9	2019/07/02 11:19:17	65.9	2019/07/02 11:21:10
48.6	2019/07/02 11:19:15	60.4	2019/07/02 11:19:12	63.7	2019/07/02 11:19:20
49.3	2019/07/02 11:19:15	62.6	2019/07/02 11:19:14	66.7	2019/07/02 11:21:09
92.9	2019/07/02 11:31:26	98.5	2019/07/02 11:31:27	97.6	2019/07/02 11:31:27

0 0.0 s # Overloads Overload Duration

Statistics LAI5.00 69.7 dB LAI10.00 67.9 dB LAI33.30 64.1 dB LAI50.00 62.2 dB 60.7 dB LAI66.60 LAI90.00 57.7 dB

Calibration History					
Preamp	Date	dB re. 1V/Pa	6.3	8.0	10.0
PRM831	2019-07-02 10:55:36	-27.7	68.6	64.6	51.9
PRM831	2019-07-02 10:06:39	-27.8	46.5	45.9	42.4
PRM831	2019-07-02 09:03:47	-27.8	58.2	64.9	63.3
PRM831	2019-06-13 09:39:04	-27.8	66.9	69.7	55.0
PRM831	2019-06-06 09:54:09	-27.8	54.5	56.4	64.1
PRM831	2019-06-06 09:53:46	-27.8	50.2	48.1	52.6
PRM831	2019-06-05 19:18:32	-27.7	58.2	56.4	51.0
PRM831	2019-06-05 19:13:22	-27.7	53.0	55.2	54.7
PRM831	2019-06-05 11:53:15	-27.9	63.3	57.9	60.0
PRM831	2019-04-18 13:26:43	-27.8	60.1	51.2	50.0
PRM831	2019-03-22 11:28:03	-27.6			

	1/
I-29 / 85th St (noise monitoring)	16
Date: July 2, 2019 Photos Taken: Yes/No	
Location: 42-85454 (east end) Calibration of Unit; Yes/No	
GPS Coordinates: $43.47546^{\circ} - 96.79760^{\circ}$	
Start time: 11:02 am  Finish time: 11:32 am  partly cloud	4
831-Data . 008	R(N)
Vehicle Count	Total
NB JANA HARAMANA HALAMANA IN INTINI INTININI INTININI INTINININI INTINININI INTINININI	141
passenger car	
53 MARTHAM CHILLIAN AND AND AND AND AND AND AND AND AND A	106
NB III	3
single-unit truck	1
SB III	4
NB	
bus	_
Siz Inkulu IIII (C)	
NB HAMMINIM (2)	21
semi truck / heavy truck	1. 1
Total (4)	14
Site Set-up Diagram  Noise Comments	
*	
7.19	
Deff of	
gother B	
(Gilboor)	
*	

7	1
4	1
1	6

1-29 / 85th St (noise monitori	ng)	16
Date:	Photos Taken: Yes/No	_
Location:	Calibration of Unit: Yes/No	
GPS Coordinates:		
Start time:		
Finish time:		
Vehicle Count  NB  passenger car		Total
NB single-unit truck	The second to the test of the state of the s	93
SB		3
NB bus		
5 B		_
NB		15
semi truck / heavy truck		
93		22
Total	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
Site Set-up Diagram	Noise Comments	

2	1
	11
	16

I-29 / 85th St (noise monitori	ng)	16
Date:	Photos Taken: Yes/No	
Location:	Calibration of Unit: Yes/No	
GPS Coordinates:		
Start time:		
Finish time:		
Vehicle Count		Total
NB	We fiff the the control of the of the officer of the continue of the control of t	115
passenger car	Constant with the American Constant of the Con	
50		1 98
NB		2
single-unit truck		
9B		2
NB		_
bus		
98		_
NA		12
semi truck / heavy truck		
99		11
Total		
Site Set-up Diagram	Noise Comments	

4/6

1-29 / 65th St (noise monitori		/ 🛇
Date:	Photos Taken: Yes/No	
Location:	Calibration of Unit: Yes/No	
<b>GPS Coordinates:</b>		
Start time:		
Finish time:		
	<u> </u>	93)
Vehicle Count	MMAN TO THE TOTAL PROPERTY OF THE PROPERTY OF	Total
NB		
-	They are the fill of the first that yill for any and the second of the s	1/02
passenger car	THE TAXABLE PART OF THE PROPERTY OF THE PROPER	1,1111
7.7		92
NB		17
single-unit truck		1
4B		2
NO		\
bus		1
6B		
110		1.0
semi truck / heavy truck	1,1 [ 1/ [ [ ] ] 1/ [ ] [ ]	15
Seilli truck / fleavy truck		
Α'/		13
Total Site Set-up Diagram		
Site Set-up Diagram	Noise Comments	

5/6

I-29 / 85th St (noise monitoring	g)		(6
Date:		Photos Taken: Yes/No	
Location:		Calibration of Unit: Yes/No	
GPS Coordinates:			
Start time:			
Finish time:			
Vehicle Count	HIMMAN S		Total
1	MIMORCHILL (IN CITIES) INTER	. And the transfer of the territorial properties of the first of the f	104
passenger car	MULLIN MILLIN MI		83
single-unit truck			1
Single-unit truck			2
NB bus			2
5B			_
semi truck / heavy truck	(\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		22 10
Total	11/1/1/1/		ΙΨ
Site Set-up Diagram		Noise Comments	

	83	31_Data,098	E	>/.
I-29 / 85th St (noise monitoring)		,		16
Date:			Photos Taken: Yes/No	0
Location:			Calibration of Unit: Yes/No	
GPS Coordinates:				
Start time:				
Finish time:				
		1	1. 111	
Vehicle Count		JULI I I I I I I I I I I I I I I I I I I		Total
NB III		11/1///////////////////////////////////	11111	61
passenger car	wa	11.1		
98 111				51
NB		in the same of the		-
single-unit truck				
98				(
NB				_
bus				
90	1.1.			_
NB 111				7
semi truck / heavy truck	1			
93			0	7
Total	1 1			
Site Set-up Diagram		Noise Comments		



Site M2: 270<sup>th</sup> Street, west of I-29 SB Camera Facing East (07/02/2019)

Monitor Location 3: File Name on Meter 831 Data.009 SLM\_0004132\_831\_Data\_009.00.ldbin NW Quadrant of 85th St and Tallgrass Ave Intersection File Name on PC Serial Number 0004132 Coords: 43° 28' 32.3"N 096° 47' 15.8"W Model Model 831 Traffic (Cars/MT/HT estimated hourly from short count): Firmware Version 2.314 Justin Anibas NB - 23 / 0 / 0 Location SB - 33 / 0 / 0 Job Description 85th Street Interchange Project EB-12/0/0 Note WB-0/0/4 Measurement Description 2019-07-02 12:04:48 Start 2019-07-02 12:34:49 Stop 00:30:01.0 . Duration Run Time 00:27:52.6 Pause 00:02:08.4 Pre Calibration 2019-07-02 12:02:59 Post Calibration None Calibration Deviation Overall Settings RMS Weight A Weighting Peak Weight A Weighting Detector Fast PRM831 Preamp Microphone Correction Off Linear Integration Method Gain 0.0 dB Overload 145.1 dB A 77.7 **C** 74.7 **z** 79.7 dB Under Range Peak Under Range Limit 26.9 27.5 33.7 dB Noise Floor 17.8 18.4 24.0 dB Results LAeq 53.1 LAE 85.4 EΑ 38.178 uPa<sup>2</sup>h 2019-07-02 12:27:28 LApeak (max) 84.3 dB LAFmax 2019-07-02 12:27:10 70.0 dB LAFmin 2019-07-02 12:14:43 37.4 dB 99.9 dB SEA LAF > 65.0 dB (Exceedance Counts / Duration) 10 16.3 s LAF > 85.0 dB (Exceedance Counts / Duration) LApeak > 135.0 dB (Exceedance Counts / Duration) 0 0.0 s 0.0 s LApeak > 137.0 dB (Exceedance Counts / Duration) 0 0.0 s LApeak > 140.0 dB (Exceedance Counts / Duration) 0 0.0 s Community Noise LEvening 19:00-23:00 Ldn LDay 07:00-23:00 LNight 23:00-07:00 LDay 07:00-19:00 53.1 53.1 53.1 65.6 dB **LC**eq 53.1 dB 12.4 dB LAeq LCeg - LAeg LAleq 55.1 dB LAeq 53.1 dB LAlea - LAea 2.0 dB Α dB Time Stamp dB Time Stamp dB Time Stamp 53.1 67.2 81.1 2019/07/02 12:20:32 2019/07/02 12:20:29 2019/07/02 12:20:32 LS(max) 68.0 80.6 70.0 2019/07/02 12:27:10 83.0 2019/07/02 12:20:32 83.5 2019/07/02 12:20:32 LF(max) 74.0 2019/07/02 12:27:10 83.6 2019/07/02 12:20:32 84.2 2019/07/02 12:20:32 LI(max) 38.7 2019/07/02 12:14:49 2019/07/02 12:05:43 58.4 2019/07/02 12:14:46 LS(min) LF(min) 37.4 2019/07/02 12:14:43 52.3 2019/07/02 12:08:23 55.7 2019/07/02 12:14:42 LI(min) 38.7 2019/07/02 12:14:49 55.9 2019/07/02 12:06:21 59.6 2019/07/02 12:10:58 LPeak(max) 84.3 2019/07/02 12:27:28 90.0 2019/07/02 12:20:28 90.5 2019/07/02 12:20:28 # Overloads 0 Overload Duration 0.0 s

 Statistics

 LAI5.00
 57.7 dB

 LAI10.00
 56.5 dB

 LAI33.30
 52.1 dB

 LAI50.00
 47.9 dB

 LAI66.60
 44.4 dB

 LAI90.00
 41.1 dB

Calibration History					
Preamp	Date	dB re. 1V/Pa	6.3	8.0	10.0
PRM831	2019-07-02 12:02:56	-27.7	51.2	46.5	47.5
PRM831	2019-07-02 10:55:36	-27.7	68.6	64.6	51.9
PRM831	2019-07-02 10:06:39	-27.8	46.5	45.9	42.4
PRM831	2019-07-02 09:03:47	-27.8	58.2	64.9	63.3
PRM831	2019-06-13 09:39:04	-27.8	66.9	69.7	55.0
PRM831	2019-06-06 09:54:09	-27.8	54.5	56.4	64.1
PRM831	2019-06-06 09:53:46	-27.8	50.2	48.1	52.6
PRM831	2019-06-05 19:18:32	-27.7	58.2	56.4	51.0
PRM831	2019-06-05 19:13:22	-27.7	53.0	55.2	54.7
PRM831	2019-06-05 11:53:15	-27.9	63.3	57.9	60.0
PRM831	2019-04-18 13:26:43	-27.8	60.1	51.2	50.0

I-29 / 85th St (no	ise monitoring)		
Da	ise monitoring) ise: July 7,2019 in: \$3-85th St. (just west of Tallgrass) ise: 43,47564 (N) 96,78773 (W) ine: 12:04pm	Photos Taken: Yes/No	
Locatio	m: \$3'-85th St. (just west of Tallgrass)	Calibration of Unit: Yes/No	
GPS Coordinat	43,47564 (N) $96,78773$ (W)	Weather: 810	4
		partly clo	vdy.
Finish tin	B31_Data. ΦΦ9	partly clo	ush (N)
	831_Data, 447	ich be	,
	Vehicle Count N – IX I	Tall gross file wind 2-50	
e	IN N/S - ILH UM I COUNTS SIS	1. No. 05/0	11
seng	1N + N/S - 1H (H) 1 (C) 90"	Jerge .	11
passenger			
	N>E-IHT		5
single-unit truck			
ıgle-uı truck			
sing			
<u>ν</u>			
snq			
ᇫ >	sidedumps of 11		2
emi trucl / heavy truck			
semi truck / heavy truck			
ν .	Total		
Site Set-up Diag		Noise Comments	
4		+3:40 - paused to talk to homeowner	
	( B)	+12:15 - paused to talk to guy driving by looking	for Minusch
10	William ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	passed to fair is goy activing by contract	J sor princesora
	Con Jacobs (May	+16:35 - displane flew over	
	$\mathcal{D}_{1}$	+ 18:49 - side dump unloaded dirt (GE corner of 80	Tallovasa)
-	85th st (gravel)	+21:25 - mover started @ NE corner of 85th/Tal	grass)(end of
,	Pallaras (2196)	+12: pp- side dump unloaded dirt (same locatio	n) record
		+28:25-airplane flew over	
	Si ge		
1	\ \ \		l



Site M3: 85<sup>th</sup> Street, east of Tallgrass Avenue Camera Facing South (07/02/2019)

Summary File Name on Meter 831 Data.010 File Name on PC

SLM\_0004132\_831\_Data\_010.00.ldbin 0004132 Model 831

2.314

Firmware Version

Justin Anibas Location

Job Description 85th Street Interchange Project Note

Monitor Location 4:

Avera Hospital Grounds, South of I-229

Coords: 43° 29' 30.3"N 096° 46' 53.5"W

Traffic (Cars/MT/HT estimated hourly from short count):

NB - 1118 / 52 / 38 SB - 1210 / 52 / 38

Measurement

Serial Number

Model

Description

2019-07-02 13:13:20 Start 2019-07-02 13:43:37 Stop Duration 00:30:17.0 Run Time 00:29:57.1 00:00:19.9 Pause

Pre Calibration 2019-07-02 13:08:23 Post Calibration None **Calibration Deviation** 

Overall Settings RMS Weight

A Weighting Peak Weight A Weighting Detector Fast PRM831 Preamp Microphone Correction Off Linear Integration Method 0.0 dB Gain Overload 145.1 dB

A 77.7 **C** 74.7 **z** 79.7 dB Under Range Peak Under Range Limit 26.9 27.5 33.7 dB Noise Floor 17.8 18.4 24.0 dB

Results LAeq

64.6 LAE 97.2 EΑ 577.284 μPa²h

2019-07-02 13:27:24 LApeak (max) 95.3 dB LAFmax 2019-07-02 13:30:40 77.3 dB LAFmin 2019-07-02 13:43:33 57.9 dB

SEA 99.9 dB

LAF > 65.0 dB (Exceedance Counts / Duration) 58 852.6 s LAF > 85.0 dB (Exceedance Counts / Duration) LApeak > 135.0 dB (Exceedance Counts / Duration) 0.0 s 0.0 s 0 LApeak > 137.0 dB (Exceedance Counts / Duration) 0 0.0 s LApeak > 140.0 dB (Exceedance Counts / Duration) 0 0.0 s

**Community Noise** Ldn LDay 07:00-23:00 LNight 23:00-07:00 LDay 07:00-19:00 LEvening 19:00-23:00 64.6 64.6 64.6

LCeq 74.7 dB LAeq LCeq - LAeq 64.6 dB 10.1 dB LAleq 65.8 dB LAeq 64.6 dB LAleq - LAeq 1.2 dB

LS(max) LF(max) LI(max) LS(min) LF(min) LI(min)

LPeak(max)

LAI66.60 LAI90.00

A		С		Z	
dB	Time Stamp	dB	Time Stamp	dB	Time Stamp
64.6		74.7		75.9	
73.7	2019/07/02 13:22:47	88.5	2019/07/02 13:38:19	89.0	2019/07/02 13:38:19
77.3	2019/07/02 13:30:40	89.7	2019/07/02 13:38:19	90.3	2019/07/02 13:38:19
80.7	2019/07/02 13:30:40	90.2	2019/07/02 13:38:19	90.7	2019/07/02 13:38:19
58.4	2019/07/02 13:43:33	69.1	2019/07/02 13:14:56	71.2	2019/07/02 13:14:58
57.9	2019/07/02 13:43:33	67.8	2019/07/02 13:14:56	69.8	2019/07/02 13:15:00
58.2	2019/07/02 13:43:33	69.4	2019/07/02 13:14:52	72.2	2019/07/02 13:14:58
95.3	2019/07/02 13:27:24	96.0	2019/07/02 13:22:47	96.2	2019/07/02 13:30:40

# Overloads 0 Overload Duration 0.0 s

Statistics LAI5.00 68.2 dB LAI10.00 67.2 dB LAI33.30 65.1 dB LAI50.00 63.6 dB 62.1 dB

Calibration History					
Preamp	Date	dB re. 1V/Pa	6.3	8.0	10.0
PRM831	2019-07-02 13:08:20	-27.7	45.1	45.3	54.7
PRM831	2019-07-02 12:02:56	-27.7	51.2	46.5	47.5
PRM831	2019-07-02 10:55:36	-27.7	68.6	64.6	51.9
PRM831	2019-07-02 10:06:39	-27.8	46.5	45.9	42.4
PRM831	2019-07-02 09:03:47	-27.8	58.2	64.9	63.3
PRM831	2019-06-13 09:39:04	-27.8	66.9	69.7	55.0
PRM831	2019-06-06 09:54:09	-27.8	54.5	56.4	64.1
PRM831	2019-06-06 09:53:46	-27.8	50.2	48.1	52.6
PRM831	2019-06-05 19:18:32	-27.7	58.2	56.4	51.0
PRM831	2019-06-05 19:13:22	-27.7	53.0	55.2	54.7
PRM831	2019-06-05 11:53:15	-27.9	63.3	57.9	60.0

60.3 dB

331\_Derta. \$10

I-29 / 85th St (noise monitoring)		6
Date: 1 / Location: # 4 / Avera Heart Most	Photos Taken: Yes No Calibration of Unit: Yes No	
GPS Coordinates: N. 43.49/75 W-96.78153°		( ( ( ( ( ) )
Start time: 1/5 pm	82 deg - 2-6 mp	m (MM.)
Finish time: (-43 pm	82° deg - 2-6 mp partly cloudy	
W11113		
Vehicle Count		Total
N/E     (((1))   (((1))   (((()))   (((()))   ((	Helman Mille Wall Himmer in Brown in the man tribe in Fig.	114
passenger car	because of the theorem and the transfer of the	
5/W [[]][[][[][[][][][][][][][][][][][][][		113
$N/\mathcal{E}$ single-unit truck		8
S/W		3
N/E		_
bus		
S/W		
N/E ILIL		5
semi truck / heavy truck		1
Total		4
Site Set-up Diagram	Noise Comments	
A N	- duration - (minor const. @ silot)	
N	- duration - (minor const. @pilot.) (harling out dist)	
1.229	Chaoting of the Co	
(x) P.lox		
N. Centrol Heart Inst. (Avera)		
Heart (not. (Avera)		

I-29 / 85th St (noise monitor Date: Location: GPS Coordinates: Start time: Finish time:	Photos Taken: Yes/No Calibration of Unit: Yes/No	46
Vehicle Count  Vehicle Count  passenger car		Total 92
single-unit truck		XIIIIIII (1 4 - 1
semi truck / heavy truck		4
Site Set-up Diagram	Noise Comments    The state of	

Date:	Photos Taken: Yes/No	
Location:		
GPS Coordinates:		
Start time:		
Finish time:		
Vehicle Count		Total
passenger car	weld Medicular in Interest recite recite receiver the fill Medicinal design and	
passeriger car		11111
ME NE		8
single-unit truck		2
		_
bus		_
NE		2
semi truck / heavy truck		4
Total		
Site Set-up Diagram	Noise Comments	

Date:	Photos Taken: Yes/No	
Location:	Calibration of Unit: Yes/No	
GPS Coordinates:		
Start time:		
Finish time:		
Vehicle Count		, , , Total, , ,
NIE		
passenger car		
1/11/5/WI	DEFORM (DO A CONTENENT EN EN EL COMMENDA (DE COLLEGE COLLEGE EN EL COLLEGE EN EL CALLEGE EN EL CALLEGE EN EL C	1000111111
NE		2
single-unit truck		
5(W		5
		-
bus		
		_
NE		4
semi truck / heavy truck	11.841	
$5 \omega$		16
Total		
Site Set-up Diagram	Noise Comments	
	tt.00 paused briefly	

I-29 / 85th St (noise monitoring)

Vehicle Count	TOTAL	
N/2	mill To	
car 5(w minimula managana mana		(1)
Single with truck Slw	6	•
NG.	10	
B== 40   N/2   11		
	4	
Frank GWI Heavy Truck		

Vehicle Court	Total
2 NE 11111111111111111111111111111111111	140
2 N(5)	23
single with track SIM	
tracic S/W !	2
NIE	and the second s
bus SIW	-
semi-trucked	-
semi-truck heavy truck SIW	-



Site M4: Avera Hospital Grounds, south of I-229 EB Camera Facing North (07/02/2019)



## Building a Better World for All of Us®

Sustainable buildings, sound infrastructure, safe transportation systems, clean water, renewable energy and a balanced environment. Building a Better World for All of Us communicates a companywide commitment to act in the best interests of our clients and the world around us.

We're confident in our ability to balance these requirements.

